

When Does a Crack Propagate?

Crack propagates if above critical stress

$$\begin{aligned} \text{i.e., } \sigma_m &> \sigma_c \\ \text{or } K_t &> K_c \end{aligned} \quad \sigma_c = \left(\frac{2E\gamma_s}{\pi a} \right)^{1/2}$$

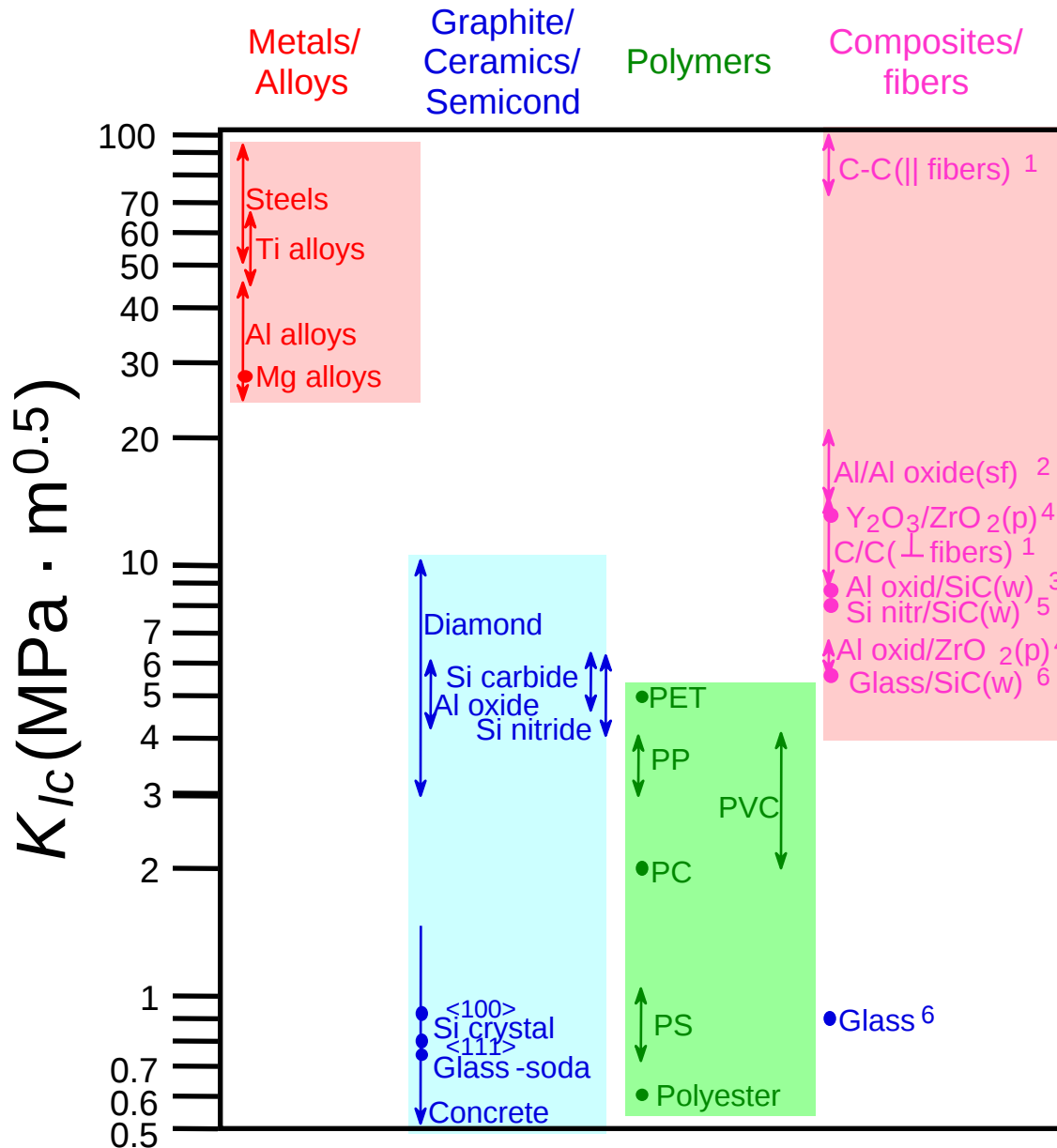
where

- E = modulus of elasticity
- γ_s = specific surface energy
- a = one half length of internal crack
- $K_c = \sigma_c / \sigma_0$

For ductile $\Rightarrow$ replace γ_s by $\gamma_s + \gamma_p$

where γ_p is plastic deformation energy

Fracture Toughness



Based on data in Table B5,
Callister 7e.

Composite reinforcement geometry is: f = fibers; sf = short fibers; w = whiskers; p = particles. Addition data as noted (vol. fraction of reinforcement):

1. (55vol%) ASM Handbook, Vol. 21, ASM Int., Materials Park, OH (2001) p. 606.
2. (55 vol%) Courtesy J. Cornie, MMC, Inc., Waltham, MA.
3. (30 vol%) P.F. Becher et al., *Fracture Mechanics of Ceramics*, Vol. 7, Plenum Press (1986). pp. 61-73.
4. Courtesy CoorsTek, Golden, CO.
5. (30 vol%) S.T. Buljan et al., "Development of Ceramic Matrix Composites for Application in Technology for Advanced Engines Program", ORNL/Sub/85-22011/2, ORNL, 1992.
6. (20vol%) F.D. Gace et al., *Ceram. Eng. Sci. Proc.*, Vol. 7 (1986) pp. 978-82.

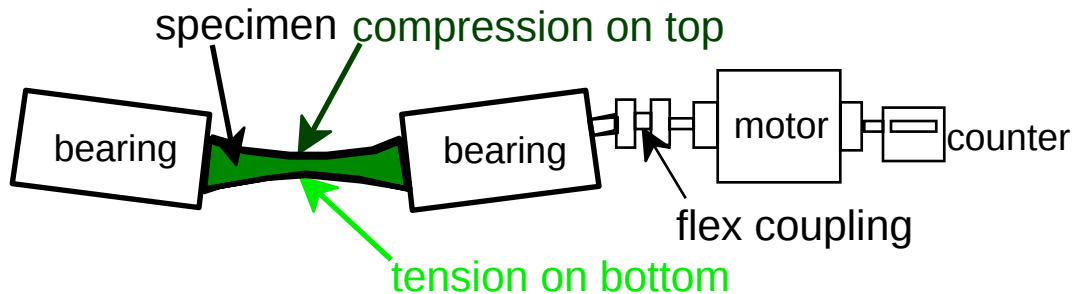
Lab Assignment

- Split into groups of 3
 - Each group gets 8 paper clips
 - Bend back and forth between zero and these angles (2 paper clips each)
 - 45
 - 90
 - 135
 - 180
 - Keep track of the number of cycles to failure for each test.



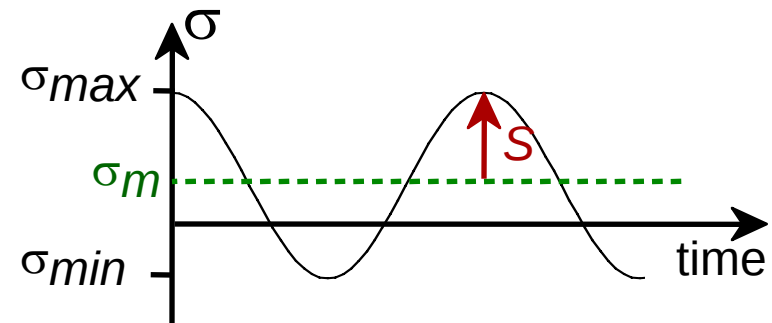
Fatigue

- **Fatigue** = failure under cyclic stress.

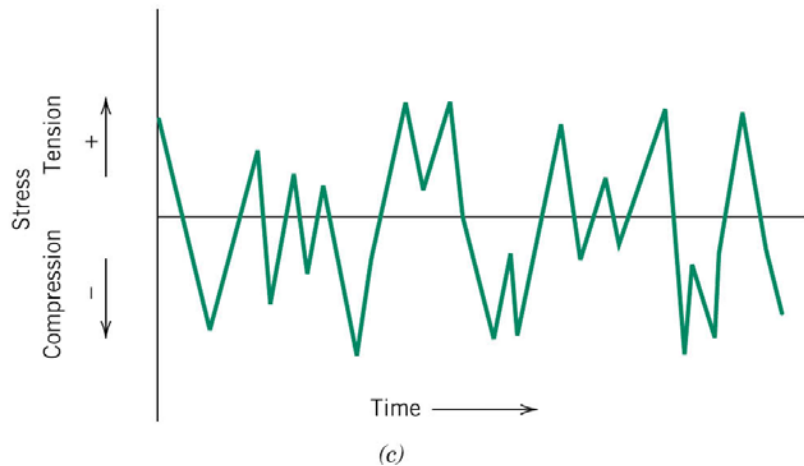
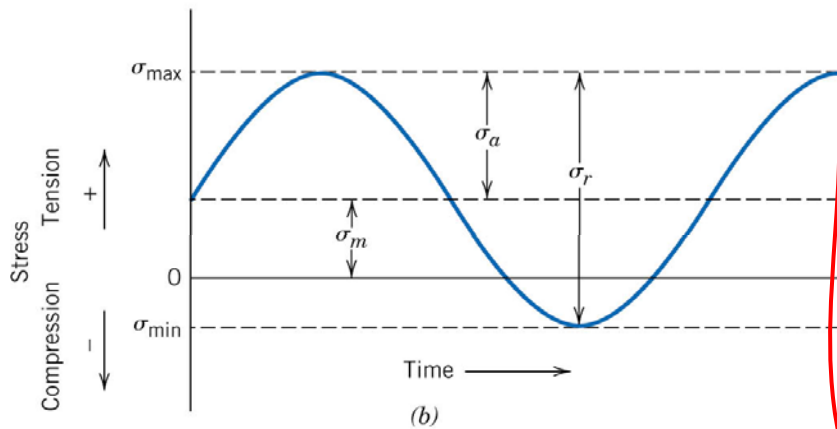
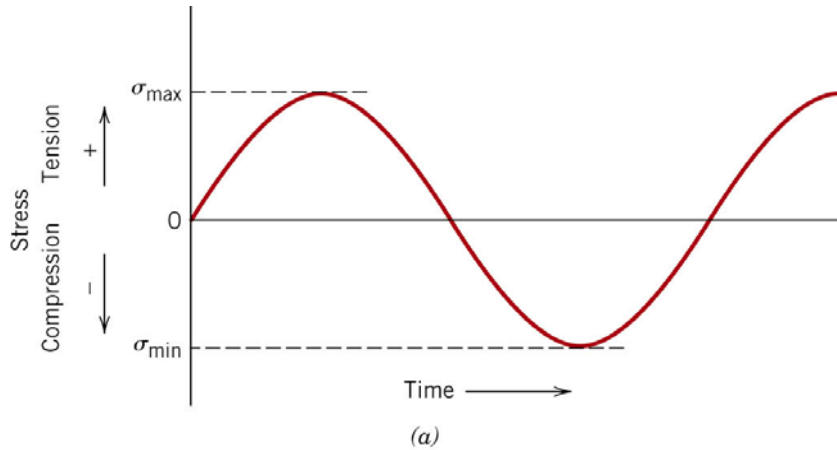


Adapted from Fig. 8.18, *Callister 7e*. (Fig. 8.18 is from *Materials Science in Engineering*, 4/E by Carl. A. Keyser, Pearson Education, Inc., Upper Saddle River, NJ.)

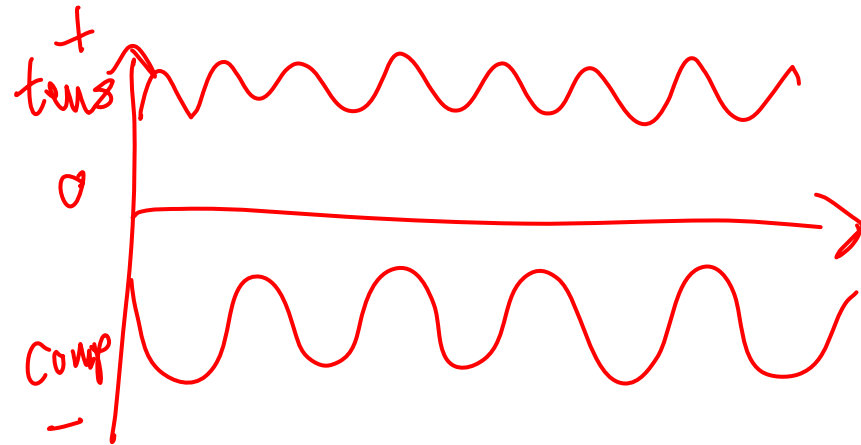
- Stress varies with time.
 - key parameters are S , σ_m , and frequency



- Key points: Fatigue...
 - can cause part failure, even though $\sigma_{max} < \sigma_c$.
 - causes ~ 90% of mechanical engineering failures.



tension - tension
comp - compression cycles



bad

not as bad

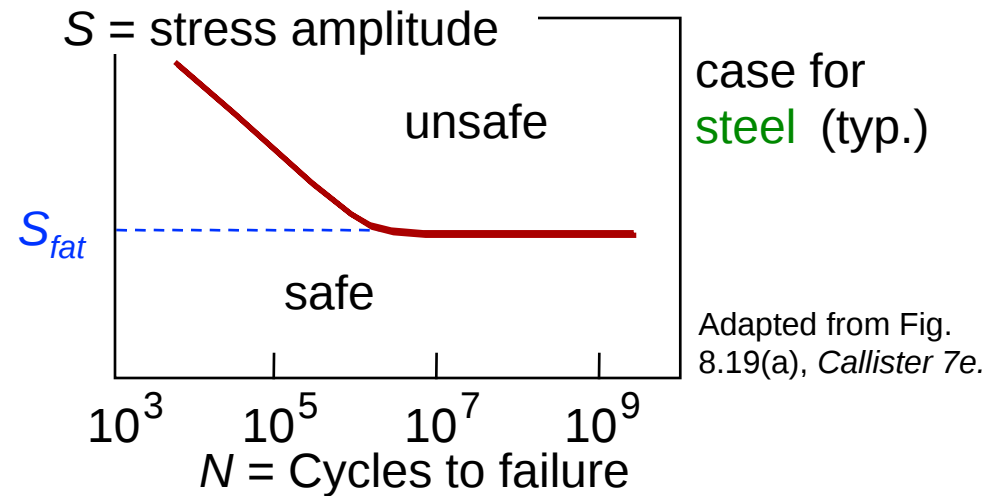
σ_s $\frac{1}{3}$ to $\frac{1}{2}$ of UTS
fracture stress

High cycle fatigue (HCF) below σ_r
 $> 10^4$ cycles
often need a flaw

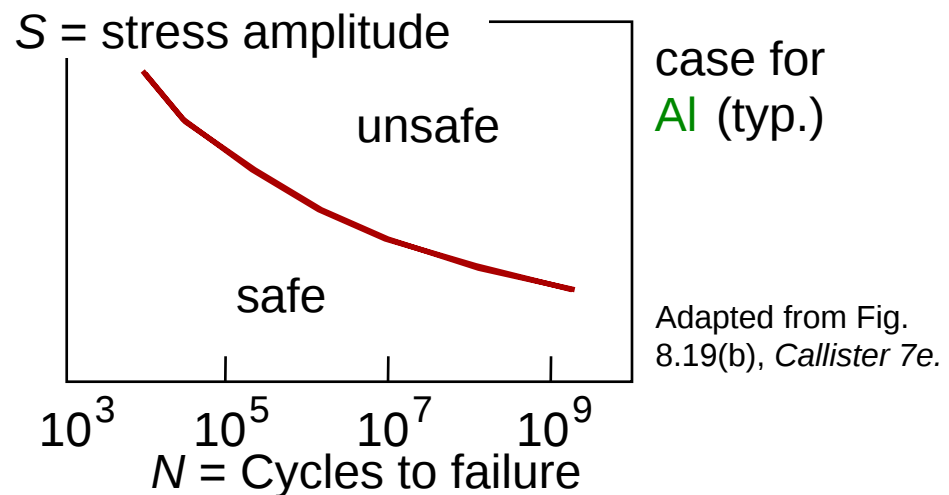
Low cycle fatigue (LCF) above σ_r
 10^4 cycles less

Fatigue Design Parameters

- Fatigue limit, S_{fat} :
--no fatigue if $S < S_{fat}$



- Sometimes, the fatigue limit is zero!



Fatigue Mechanism

- Crack grows *incrementally*

$$\frac{da}{dN} = (\Delta K)^m$$

typ. 1 to 6

$\sim (\Delta\sigma)\sqrt{a}$

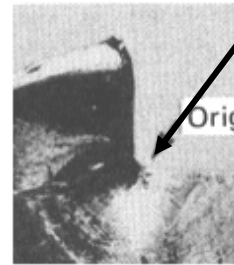
increase in crack length per loading cycle

- Failed rotating shaft
--crack grew even though

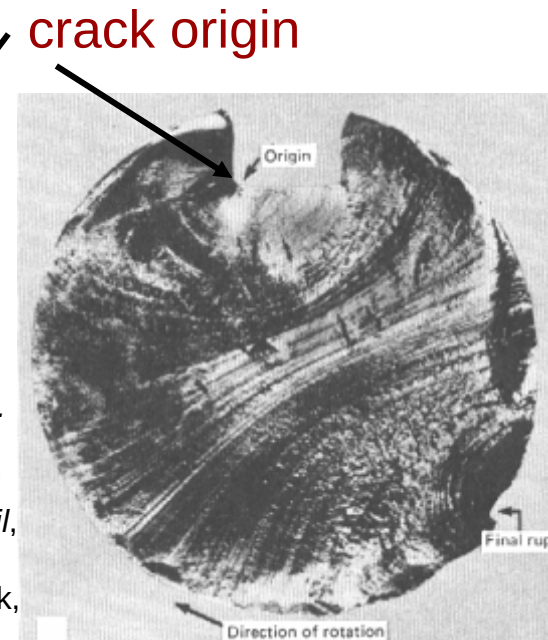
$$K_{max} < K_c$$

- crack grows faster as

- $\Delta\sigma$ increases
- crack gets longer
- loading freq. increases.

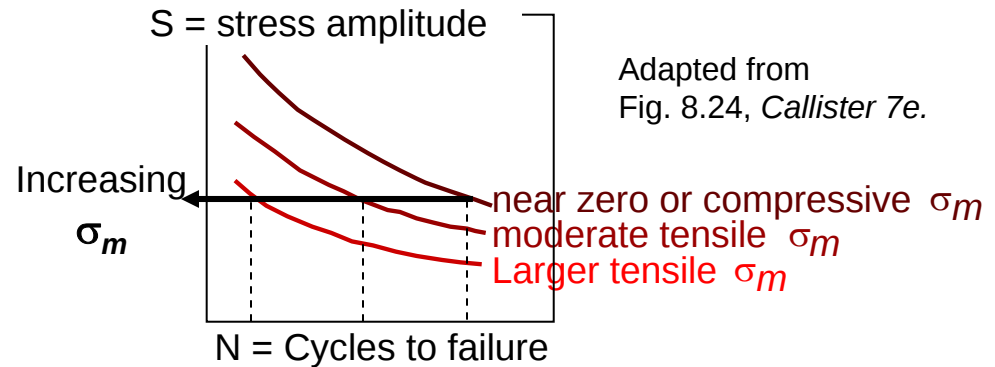


Adapted from
Fig. 8.21, Callister 7e.
(Fig. 8.21 is from D.J.
Wulpi, *Understanding
How Components Fail*,
American Society for
Metals, Materials Park,
OH, 1985.)

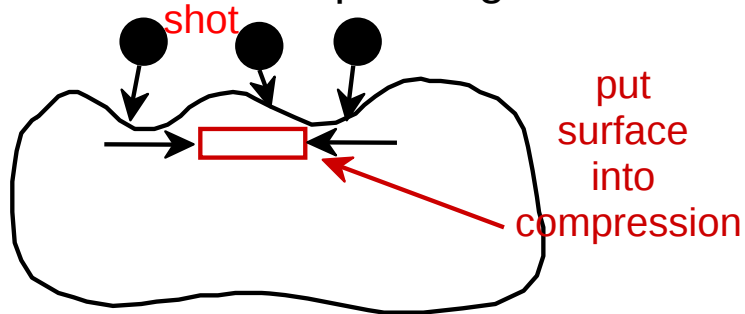


Improving Fatigue Life

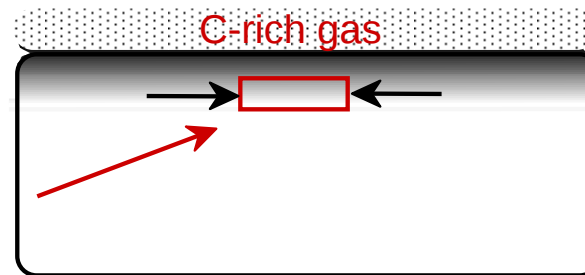
1. Impose a compressive surface stress
(to suppress surface cracks from growing)



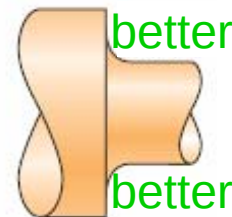
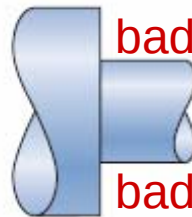
--Method 1: shot peening



--Method 2: carburizing



2. Remove stress concentrators.

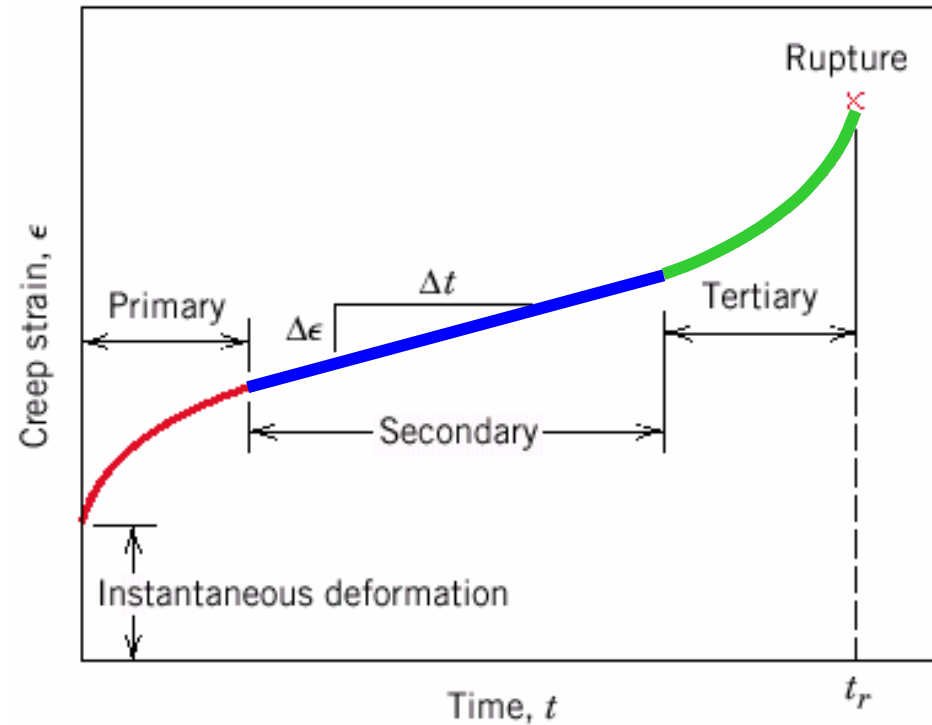
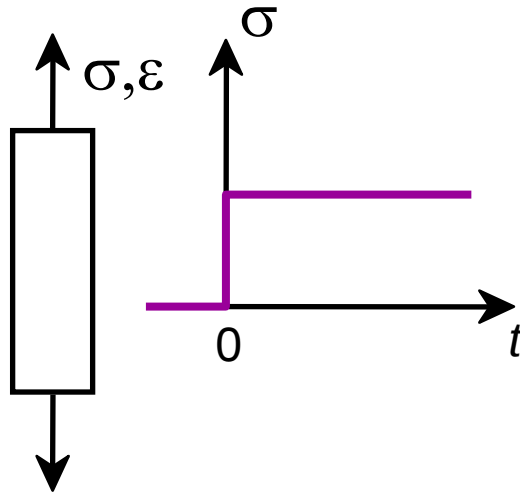


Adapted from Fig. 8.25, Callister 7e.

Creep

temp dependent

Sample deformation at a constant stress (σ) vs. time



Primary Creep: slope (creep rate) decreases with time.

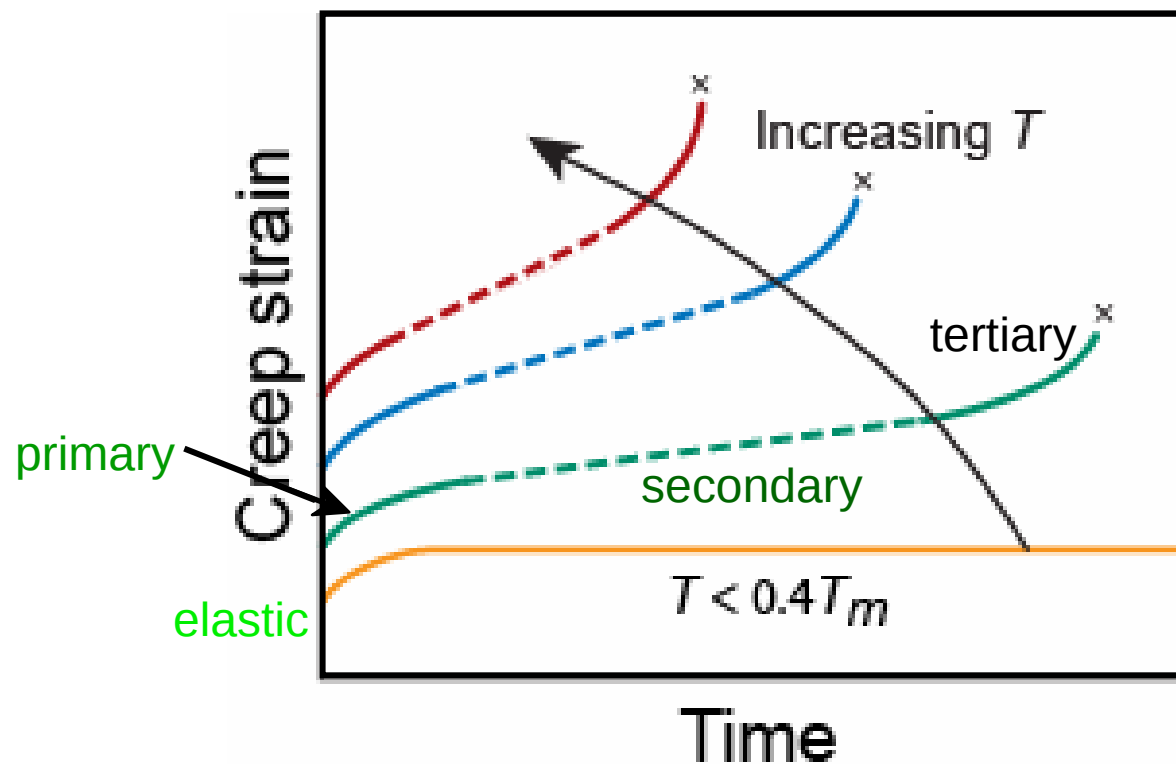
Secondary Creep: steady-state i.e., constant slope.

Tertiary Creep: slope (creep rate) increases with time, i.e. acceleration of rate.

Adapted from
Fig. 8.28, Callister 7e.

Creep

- Occurs at elevated temperature, $T > 0.4 T_m$



Adapted from Figs. 8.29,
Callister 7e.

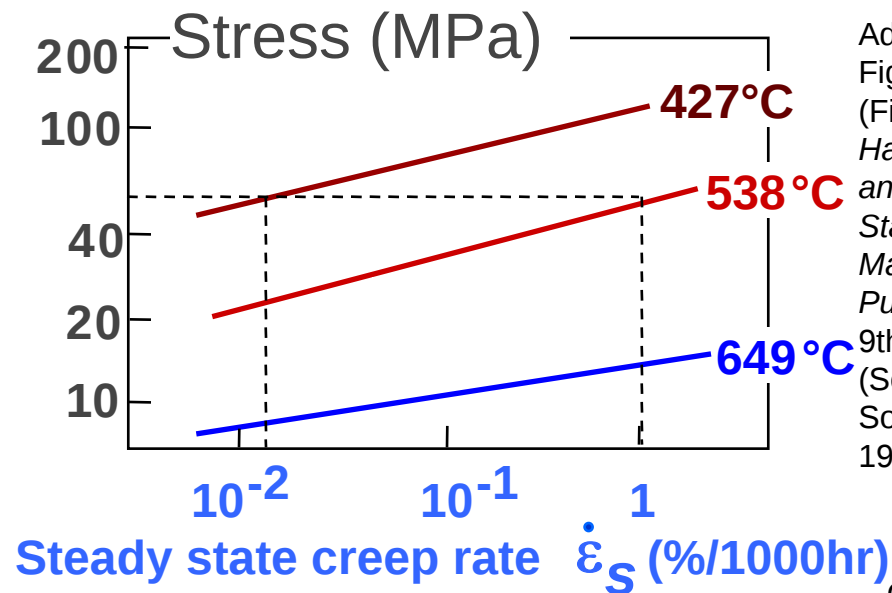
Secondary Creep

- Strain rate is constant at a given T , σ
 - strain hardening is balanced by recovery

$$\dot{\epsilon}_s = K_2 \sigma^n \exp\left(-\frac{Q_c}{RT}\right)$$

strain rate $\dot{\epsilon}_s$ (blue box)
 material const. K_2 (black box)
 stress exponent (material parameter) n (green box)
 applied stress σ (black box)
 activation energy for creep (material parameter) Q_c (red box)

- Strain rate increases for higher T , σ

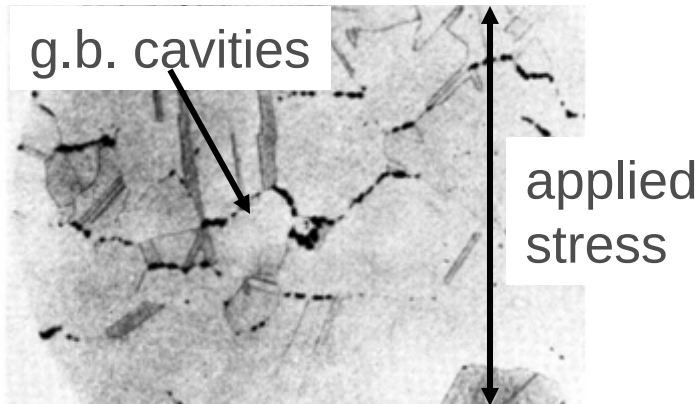


Adapted from Fig. 8.31, Callister 7e. (Fig. 8.31 is from *Metals Handbook: Properties and Selection: Stainless Steels, Tool Materials, and Special Purpose Metals*, Vol. 3, 9th ed., D. Benjamin (Senior Ed.), American Society for Metals, 1980, p. 131.)

8.14

Creep Failure

- Failure:
along grain boundaries.



From V.J. Colangelo and F.A. Heiser, *Analysis of Metallurgical Failures* (2nd ed.), Fig. 4.32, p. 87, John Wiley and Sons, Inc., 1987. (Orig. source: Pergamon Press, Inc.)

- Time to rupture, t_r

$$T(20 + \log t_r) = L$$

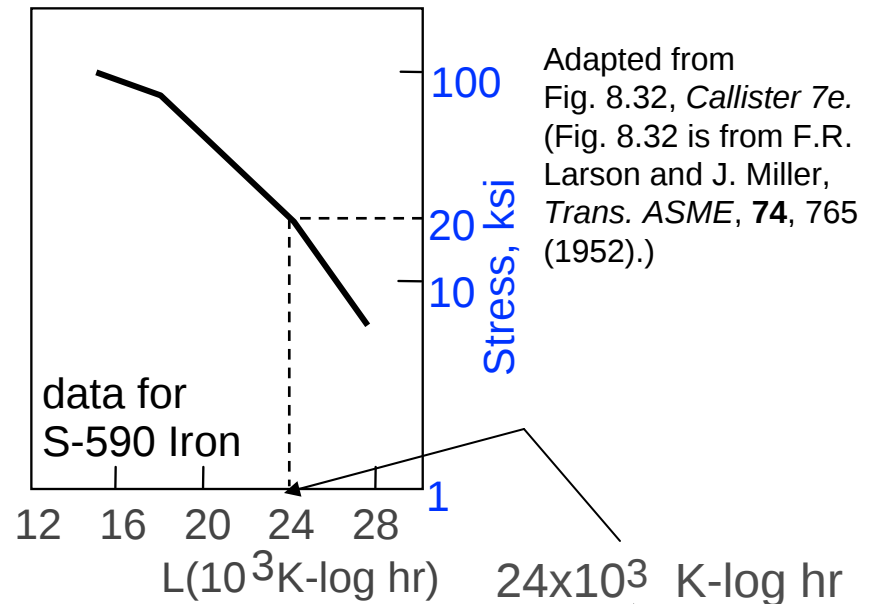
temperature

time to failure (rupture)

function of
applied stress

- Estimate rupture time

S-590 Iron, $T = 800^\circ\text{C}$, $\sigma = 20$ ksi



$$T(20 + \log t_r) = L$$

1073K

Ans: $t_r = 233$ hr

Designing for Optoelectronics

optoelectronics

- Creep resistant solders for *dimensional stability*
- Non-brittle intermetallics and smooth bonding interfaces for *long term reliability*

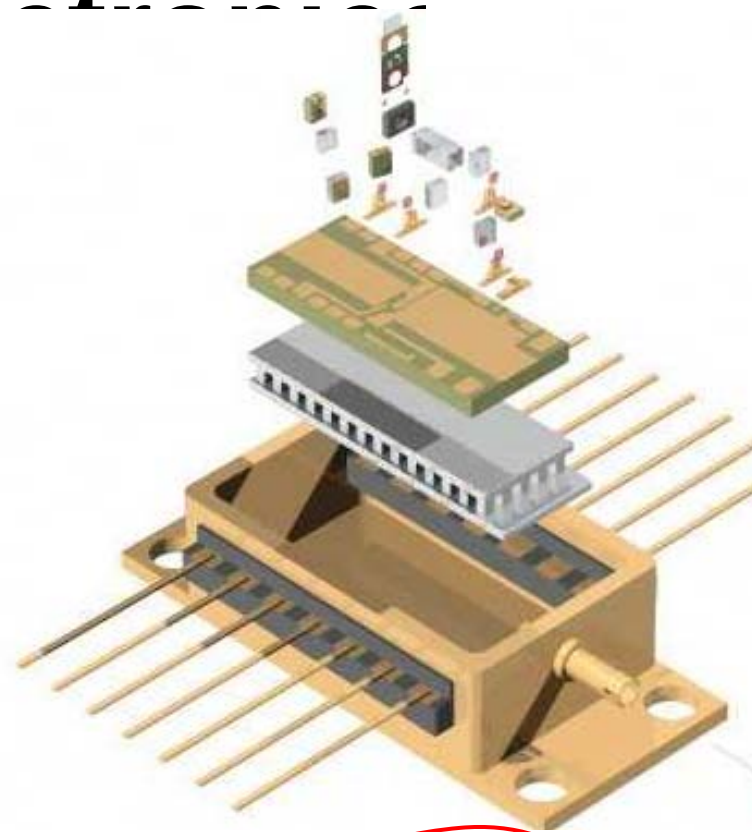
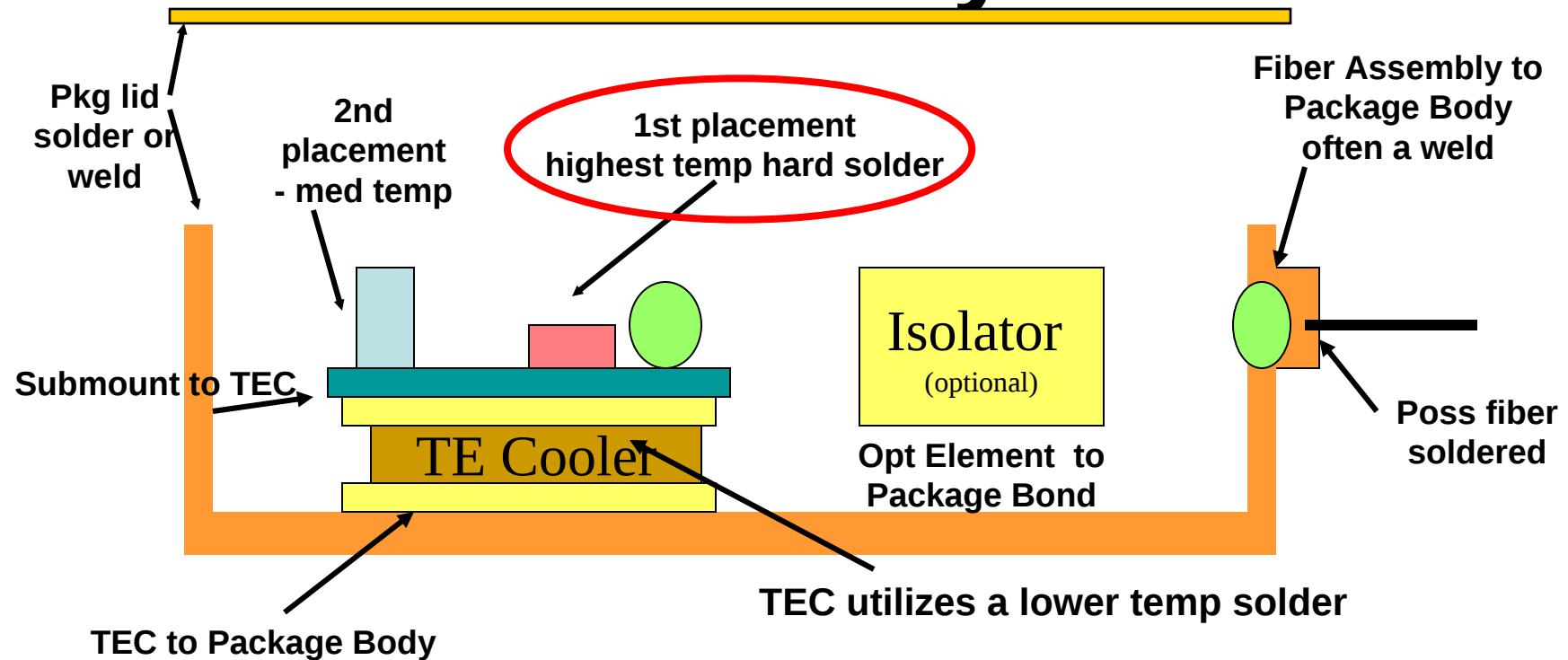


Image courtesy of Axsun, Inc.

Solders & Solder Hierarchy



Need a series of solders melting at successively lower temps

SUMMARY

Ch 8

- Engineering materials don't reach **theoretical strength**.
- **Flaws** produce **stress concentrations** that cause premature failure.
- Sharp corners produce large stress concentrations and premature failure.
- Failure type depends on T and stress:
 - for noncyclic σ and $T < 0.4T_m$, failure stress decreases with:
 - increased maximum flaw size,
 - decreased T ,
 - increased rate of loading.
 - for cyclic σ :
 - cycles to fail decreases as $\Delta\sigma$ increases.
 - for higher T ($T > 0.4T_m$):
 - time to fail decreases as σ or T increases.

Ch 8 summary

WebCT

- **Additional homework from Ch. 8**
 - 8.14, 8.15, 8.16, 8.22, 8.25, 8.26, 8.28, 8.29
- **Sections not covered, not tested**
 - 8.6, 8.15