

## Problem Set 7

**The Cascode Amplifier (Section 6.8):**

- Problem 6.105 in the textbook
- Problem 6.107 (a and c only) in the textbook

**Differential Cascode Amplifiers (Sections 6.8 and 7.5)  
and Advanced Current Mirrors (Section 6.12)**

• **Problem1:**

Figure 1 shows a differential *cascode* amplifier with an active load formed by a Wilson current mirror.

Figure 2 shows a differential *folded-cascode* amplifier with an active load formed by a modified Wilson current mirror. Both the cascode amplifier (in Figure 1) and the folded-cascode amplifier (in Figure 2) apply a differential common-base stage to the input differential pair. However, the folded-cascode amplifier uses cascode transistors opposite in type from those used in the input stage. **This arrangement of opposite-type transistors allows for the output of the amplifier to be taken at the same bias-voltage levels as the input signals.**

For the amplifiers in Figures 1 and 2:

Assume that the bias-voltage level at the output is stabilized by negative feedback (to about 0 V) and that all BJTs are in the active region. When finding the dc currents, ignore the base currents of every transistor.

**A)** What is the dc bias current in transistors  $Q_1$  and  $Q_3$  (in terms of  $I$ )?

**B)** Find an expression for:

- the amplifier input resistance  $R_i$
- the amplifier output resistance  $R_o$

Hint: the output resistance of the Wilson current mirror ( $Q_5$ - $Q_7$ ) is approximately  $\beta r_o/2$ .

- the short-circuit transconductance  $G_m$  (where  $G_m \equiv i_{\text{out}}/v_{\text{in}} \Big|_{R_L=0}$ )

and draw the equivalent transconductance circuit model of the amplifier.

- the open-circuit small-signal voltage gain  $A_v$  (where  $A_v \equiv \frac{v_{\text{out}}}{v_{\text{in}}} \Big|_{R_L=\infty}$ )

C) Assume that, for proper operation, the minimum voltage drop across any of the current sources is  $V_{CS}$ .

Find an expression for:

- the smallest value  $V_{BIAS, \min}$  of  $V_{BIAS}$  in Fig. 1, with cascode transistors  $Q5-Q7$  in the active mode.
- the largest value  $V_{BIAS, \max}$  of  $V_{BIAS}$  in Fig. 2, with cascode transistors  $Q5-Q7$  in the active mode.
- the input common-mode voltage range and the output voltage range, over which the amplifier behaves as a linear amplifier for small-signal differential inputs (i.e., over which all BJTs are in active mode).
- simplify the above expressions, assuming:

$$|V_{CS}| = |V_{CE, \text{sat}} + V_{BE, \text{on}}| \text{ and } |V_{CEsat}| = |V_{BE, \text{on}} - V_{BC, \text{on}}|$$

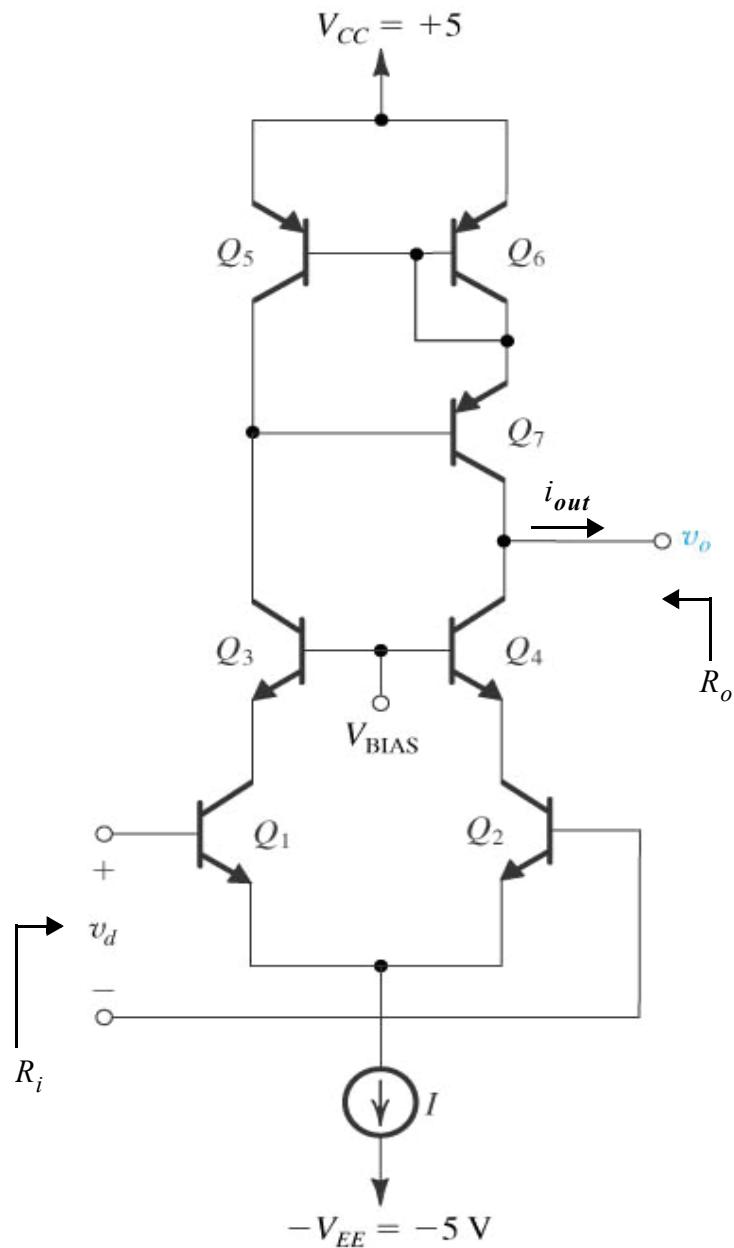


Figure 1 (Fig. P7.74)

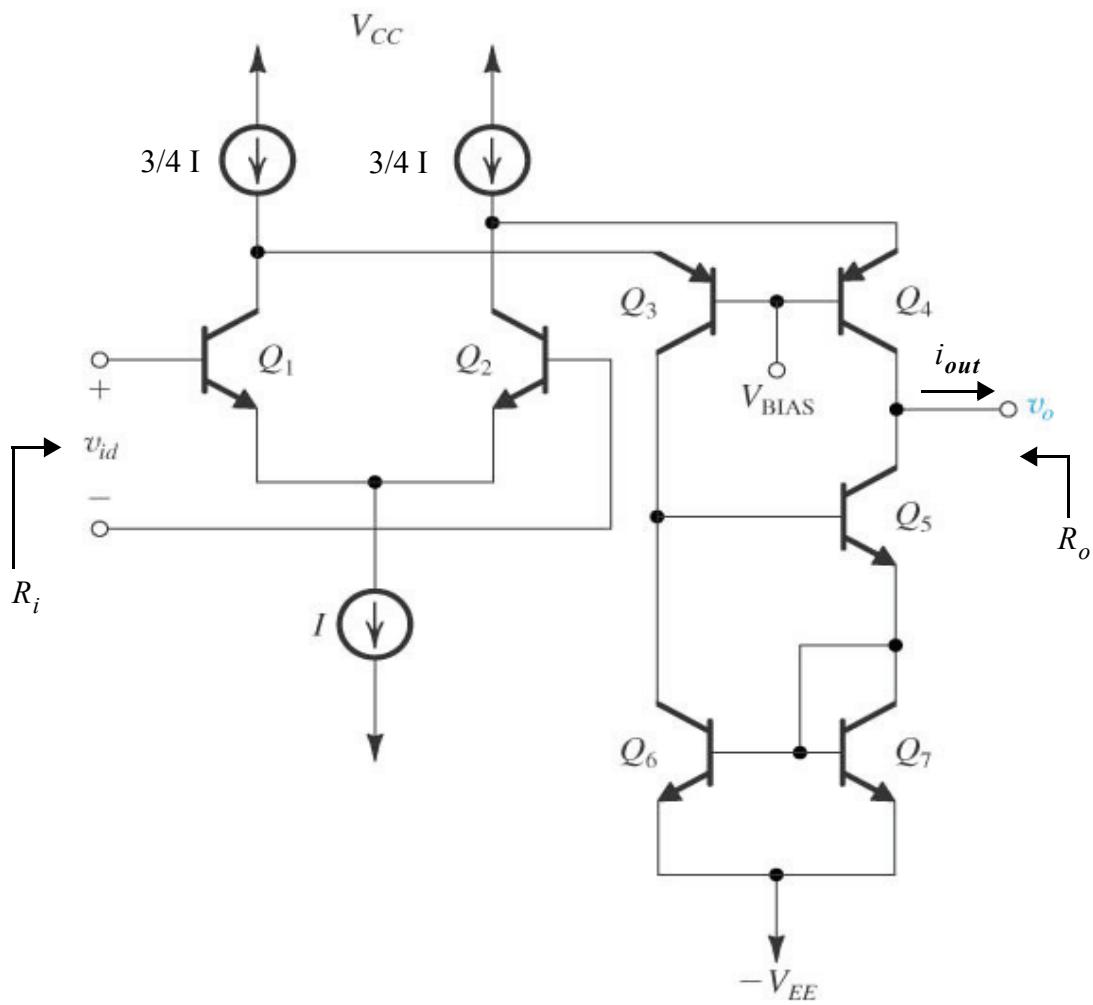


Figure 2 (Fig. 7.35)

**• Problem 2:**

**D7.75** Consider the bias design of the Wilson-loaded cascode differential amplifier shown in Fig. P7.74.(Figure 1)

- (a) What is the largest signal voltage possible at the output without  $Q_7$  saturating? Assume that the CB junction conducts when the voltage across it exceeds 0.4 V.
- (b) What should the dc bias voltage established at the output (by an arrangement not shown) be in order to allow for positive output signal swing of 1.5 V?
- (c) What should the value of  $V_{BIAS}$  be in order to allow for a negative output signal swing of 1.5 V?
- (d) What is the upper limit on the input common-mode voltage  $v_{CM}$ ?

**High-Frequency Response of Cascode Amplifiers (Sections 6.6 and 6.8 )**

• **Problem 3:**

For the amplifiers in Figures 3 and 4, derive an expression for:

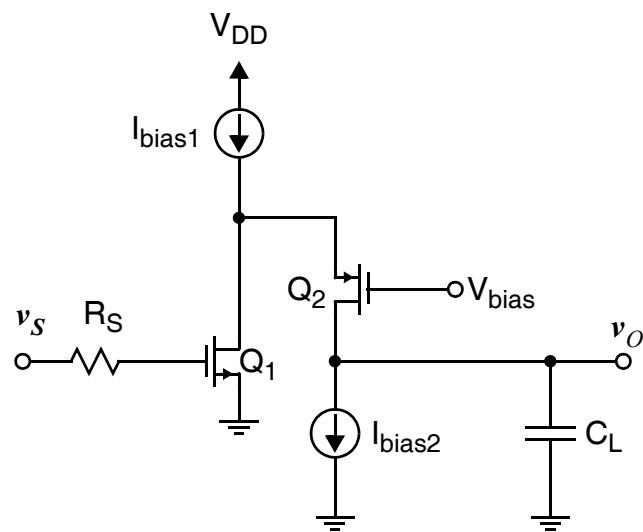
- i) the midband voltage gain  $A_M = v_o/v_s$ ;
- ii) the 3dB-frequency  $\omega_H$ , assuming a dominant pole exist.

Hint: Follow the following steps to find  $\omega_H$ :

- 1) apply Miller's theorem;
- 2) find the open-circuit time constants (poles) associated with each node;
- 3) find  $\omega_H$  based on the open-circuit time-constant approximation, assuming a dominant pole exists.

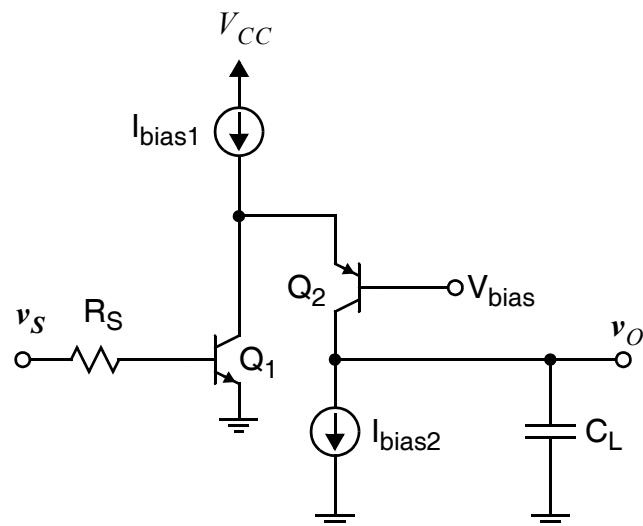
Assume:

- Biasing:
  - each current source has an output resistance of  $R_L$ .
  - the dc-bias voltage level at the output is stabilized by negative feedback, with all BJTs and MOSFETs biased in the active and saturation modes, respectively.
- For the MOS amplifiers in Figure 3.:
  - the body effect is negligible.
  - the substrate (Body) terminal of the NMOS transistors is connected to  $GND$ .
  - the substrate (Body) terminal of the PMOS transistors is connected to  $V_{DD}$ .
- For the BJT amplifiers in Figure 4:
  - neglect the small-signal base resistance  $r_x$ .



(a) MOS Folded-Cascode Amplifier

Figure 3. MOS amplifiers.



(d) BJT Folded-Cascode Amplifier

Figure 4 BJT amplifiers.