



# INTRODUCTION TO MICROELECTRONICS

## ECSE334

Wednesday, April 25, 2007, 2:00pm

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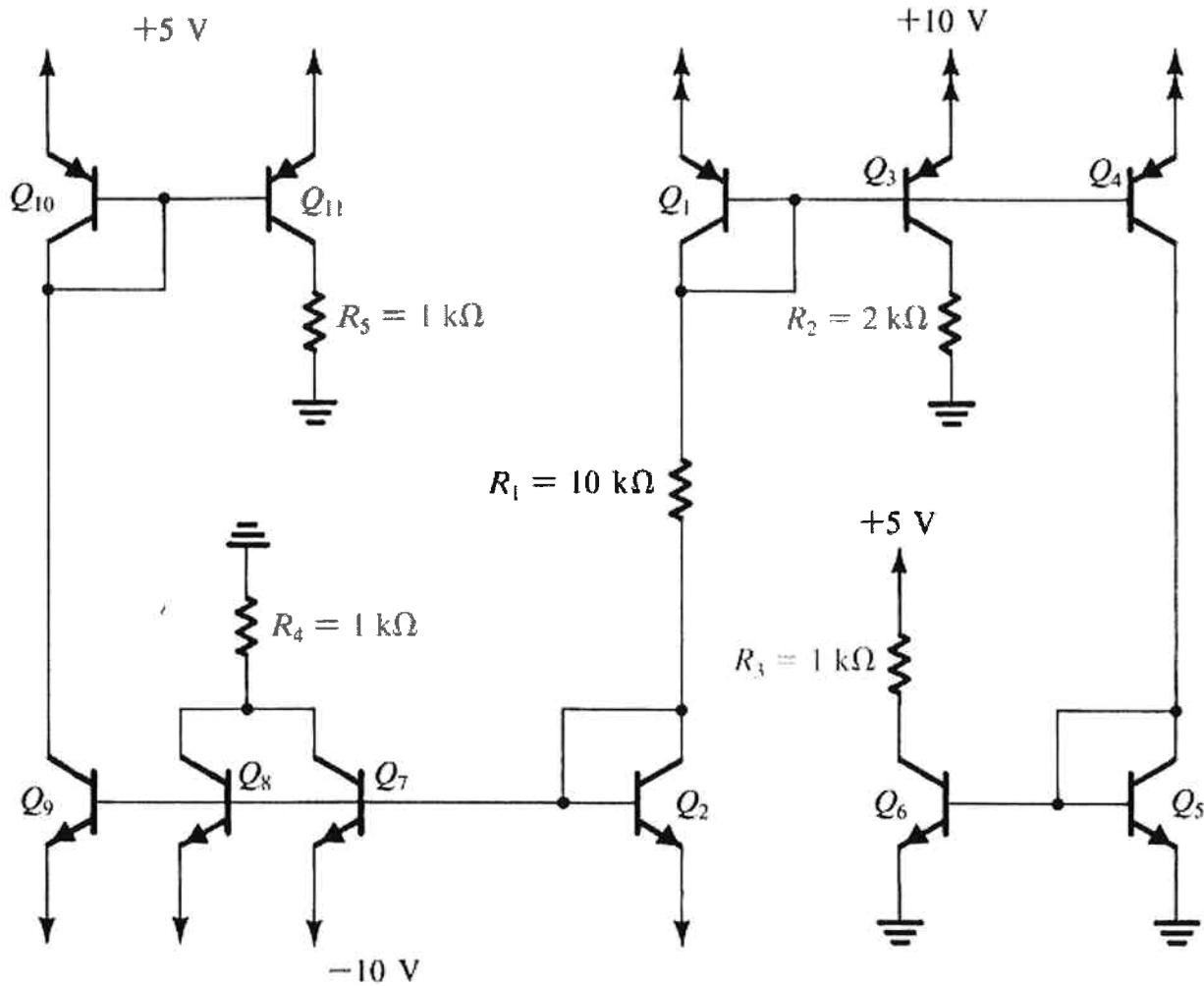
### INSTRUCTIONS

- The total number of points in this examination is 50
- This is a **closed book** examination.
- You are permitted **regular and translation dictionaries**.
- **Faculty standard calculator** permitted only.
- Answer all questions, and write your answers on the examination paper.
- This examination paper must be returned.
- A formula sheet is included at the end of the exam paper.

Question#	1	2	3	4
Weight	8	20	15	7
Score				

Total Score

**QUESTION 1:(8 MARKS)**

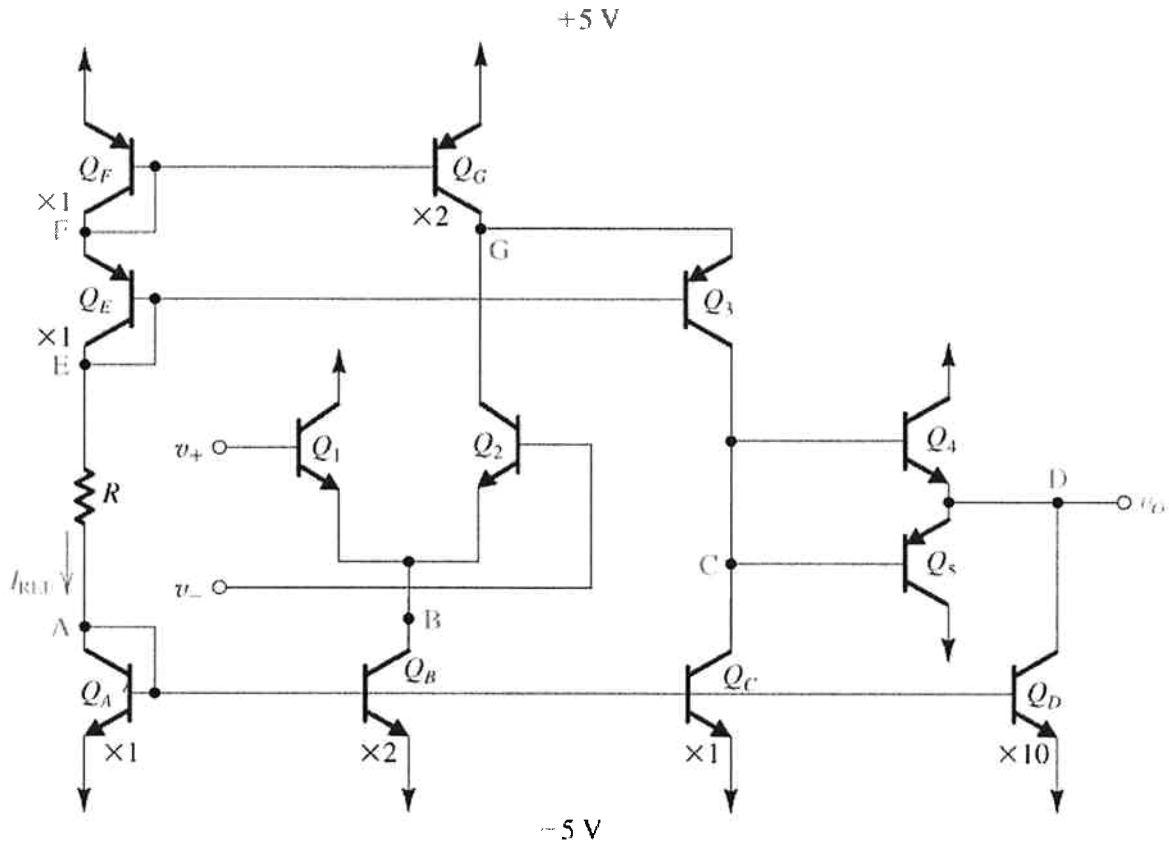


**Figure Q1.1**

Consider the circuit in Figure Q1.1. Find the current in all 5 resistors. Assume  $|V_{BE}| = 0.7\text{ V}$  and  $\beta = \infty$ .



**QUESTION 2: (20 MARKS)**



**Figure Q2.1**

The circuit shown in Figure Q2.1, is a multistage amplifier with a differential input stage. It uses a folded cascode involving transistor  $Q_3$ . Note that transistor  $Q_5$  operates in class B mode and is off at the quiescent point, while  $Q_4$  is ON at the quiescent point with  $Q_D$  sinking its bias current. All transistors have  $|V_{BE}| = 0.7V$ ,  $V_A = 200V$ , and  $\beta = 100$ .

- Perform a dc bias calculation at the quiescent point ( $v_+ = v_- = 0V$ , and  $v_o$  is stabilized by external feedback to  $0V$ ) and determine  $R$  so that the reference current  $I_{REF}$  is  $100\mu A$ . For this DC bias calculation you may assume  $|V_{BE}| = 0.7V$ , infinite  $\beta$ , and  $V_A = \infty$ . What are the dc voltages at all the labeled nodes (A, B, C, D, E, F, G).
- Provide in tabular form the bias current for all transistors. Provide  $g_m$  and  $r_o$  for the signal transistors ( $Q_1$ ,  $Q_2$ ,  $Q_3$ ,  $Q_4$ , and  $Q_5$ ), and  $r_o$  for  $Q_C$ ,  $Q_D$  and  $Q_G$ .
- Using  $\beta = 100$ , find the voltage gain  $v_o/(v_+ - v_-)$  at the quiescent point, and in the process verify the polarity of the inputs.
- Find the input and output resistances at the quiescent point ( $v_+ = v_- = 0V$ , and  $v_o$  is stabilized by external feedback to  $0V$ ).
- Find the input common mode range for linear operation.
- Under what conditions does transistor  $Q_5$  turn on?





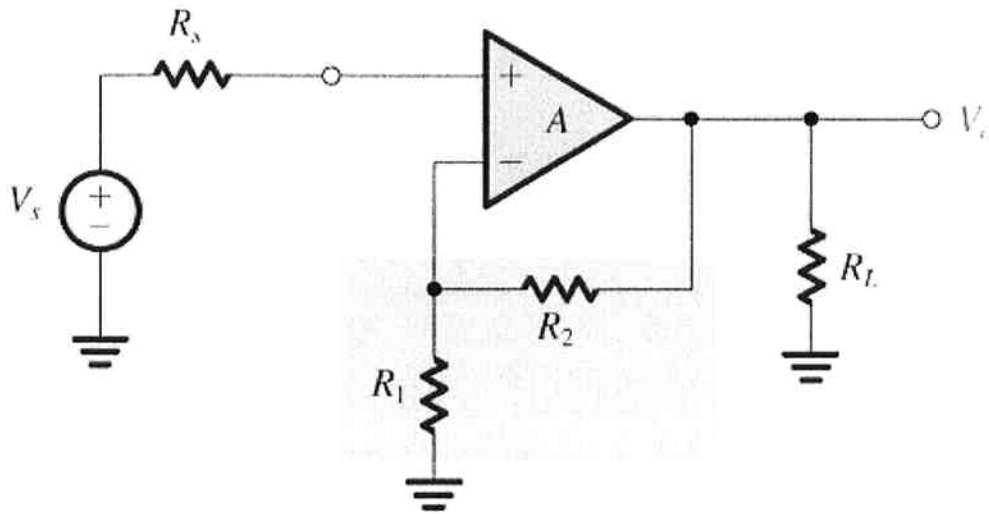








**QUESTION 3:(15 MARKS)**



**Figure Q3.1: OpAmp Circuit**

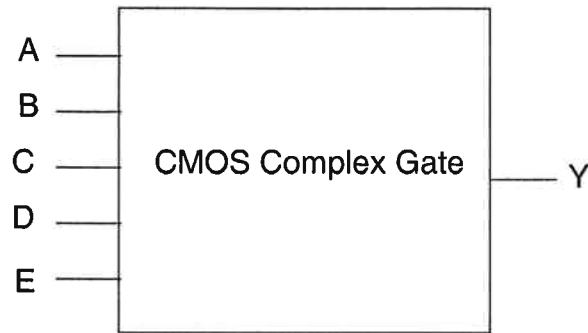
Consider the circuit in series-shunt feedback configuration shown in Figure Q3.1. Assume that the opamp has infinite input resistance, zero output resistance and a base-band gain of  $A = 10^5$ .

- Find an expression for the feedback factor  $\beta$ .
- Find the ratio  $R_2/R_1$  to obtain a closed loop voltage gain of  $A_f = \frac{V_o}{V_s} = 10$ .
- If  $A$  decreases by 20%, what is the corresponding decrease in  $A_f$ .
- If the opamp has poles at  $f_{p1} = 10^4 \text{ Hz}$ ,  $f_{p2} = 10^7 \text{ Hz}$  and  $f_{p3} = 10^8 \text{ Hz}$ , find the ratio  $R_2/R_1$  that results in at least a 45 degree phase margin.





**QUESTION 4: (7MARKS)**



**Figure Q4.1**

Draw the general topology of a complex CMOS gate that realizes the following logic function:  $Y = \overline{A \cdot B} + C \cdot (D + E)$ .



**Table 4.2 SUMMARY OF THE BJT CURRENT-VOLTAGE RELATIONSHIPS IN THE ACTIVE MODE**

$$i_C = I_S e^{v_{BE}/V_T}$$

$$i_B = \frac{i_C}{\beta} = \left(\frac{I_S}{\beta}\right) e^{v_{BE}/V_T}$$

$$i_E = \frac{i_C}{\alpha} = \left(\frac{I_S}{\alpha}\right) e^{v_{BE}/V_T}$$

Note: For the *pnp* transistor, replace  $v_{BE}$  with  $v_{EB}$ .

$$i_C = \alpha i_E \quad i_B = (1 - \alpha)i_E = \frac{i_E}{\beta + 1}$$

$$i_C = \beta i_B \quad i_E = (\beta + 1)i_B$$

$$\beta = \frac{\alpha}{1 - \alpha} \quad \alpha = \frac{\beta}{\beta + 1}$$

$$V_T = \text{thermal voltage} = \frac{kT}{q} \approx 25 \text{ mV at room temperature}$$

**Table 4.3 RELATIONSHIPS BETWEEN THE SMALL-SIGNAL MODEL PARAMETERS OF THE BJT**

Model Parameters in Terms of DC Bias Currents:

$$g_m = \frac{i_C}{V_T} \quad r_e = \frac{V_T}{I_E} = \alpha \left(\frac{V_T}{I_C}\right)$$

$$r_\pi = \frac{V_T}{I_B} = \beta \left(\frac{V_T}{I_C}\right) \quad r_o = \frac{V_A}{I_C}$$

In terms of  $g_m$ :

$$r_e = \frac{\alpha}{g_m} \quad r_\pi = \frac{\beta}{g_m}$$

In terms of  $r_e$ :

$$g_m = \frac{\alpha}{r_e} \quad r_\pi = (\beta + 1)r_e \quad g_m + \frac{1}{r_\pi} = \frac{1}{r_e}$$

Relationships between  $\alpha$  and  $\beta$ :

$$\beta = \frac{\alpha}{1 - \alpha} \quad \alpha = \frac{\beta}{\beta + 1} \quad \beta + 1 = \frac{1}{1 - \alpha}$$

**Table 5.4 SUMMARY OF IMPORTANT MOSFET EQUATIONS**

**Current-Voltage Relationships**

■ For NMOS Devices:

- Triode region ( $v_{GS} \geq V_t$ ,  $v_{DS} \leq v_{GS} - V_t$ )

$$i_D = k'_n \left( \frac{W}{L} \right) \left[ (v_{GS} - V_t)v_{DS} - \frac{1}{2} v_{DS}^2 \right]$$

$$\text{For small } v_{DS}: r_{DS} = \frac{v_{DS}}{i_D} = \left[ k'_n \left( \frac{W}{L} \right) (v_{GS} - V_t) \right]^{-1}$$

- Saturation region ( $v_{GS} \geq V_t$ ,  $v_{DS} \geq v_{GS} - V_t$ )

$$i_D = \frac{1}{2} k'_n \left( \frac{W}{L} \right) (v_{GS} - V_t)^2 (1 + \lambda v_{DS})$$

- $k'_n = \mu_n C_{ox}$  (see Table 5.1)

$$V_t = V_{t0} + \gamma [\sqrt{2\phi_f} + |V_{SB}|] - \sqrt{2\phi_f}$$

$$\gamma = \sqrt{2qN_A \epsilon_s / C_{ox}} \quad q = 1.6 \times 10^{-19} \text{ coulomb, } \epsilon_s = 1.04 \times 10^{-12} \text{ F/cm}$$

$$\lambda = 1/V_A, \quad V_A \propto \alpha L$$

■ For PMOS Devices:  $V_t$ ,  $\gamma$ ,  $\lambda$  and  $V_A$  are negative

- For triode region,  $v_{GS} \leq V_t$  and  $v_{DS} \geq v_{GS} - V_t$
- For saturation region,  $v_{GS} \leq V_t$  and  $v_{DS} \leq v_{GS} - V_t$

■ For Depletion Devices (refer to Fig. 5.23):

- $n$  channel:  $V_t$  is negative
- $p$  channel:  $V_t$  is positive

$$I_{DSS} = \frac{1}{2} k' \left( \frac{W}{L} \right) V_t^2$$

**Small-Signal Model (Fig. 5.67)**

$$g_m = \sqrt{2k'(W/L)} \sqrt{I_D} \quad r_o = \frac{|V_A|}{I_D}$$

$$g_m = k'(W/L)(V_{GS} - V_t)$$

$$g_m = \frac{2I_D}{V_{GS} - V_t} \quad V_{GS} - V_t = V_{eff}$$

$$g_{mb} = \chi g_m, \quad \chi = \gamma / [2\sqrt{2\phi_f} + |V_{SB}|]$$

$$C_{gs} = \frac{2}{3} WLC_{ox} + WL_{ov}C_{ov} \quad C_{gd} = WL_{ov}C_{ov}$$

$$C_{sb} = \frac{C_{sb0}}{\sqrt{1 + \frac{|V_{SB}|}{V_0}}} \quad C_{db} = \frac{C_{db0}}{\sqrt{1 + \frac{|V_{DB}|}{V_0}}}$$

$$f_T = \frac{g_m}{2\pi(C_{gs} + C_{gd})}$$