# **McGill University**

Faculty of Engineering
Department of Electrical and Computer Engineering

Final Examination: Electronic Circuits I - ECSE-330B

April 11<sup>th</sup> 2006, 2:00 PM - 5:00 PM

Examiner: Dr. Ramesh Abhari;

Associate Examiner: Dr. Gordon Roberts;

## **Instructions:**

- 1) This is a closed-book examination, no notes permitted. There are 2 pages of equations provided at the end of the questions.
- 2) The examination consists of 7 problems with the total possible points of 50. Partial point distribution is indicated in brackets.
- 3) The examination consists of 10 pages, including this page and the equation pages; please ensure you have a COMPLETE exam book.
- 4) Only the Faculty Standard Calculator is permitted.
- 5) Write your answers in the provided Answer Booklets.
- 6) Show your work: Answers without justification will not receive marks. State any assumption you find necessary to complete your answer.

Last Name	
First Name	
Student Number	

Question	1	2	3	4	5	6	7
Mark	/3	/6	/5	/7	/11	/8	/10
TOTAL	/:	50			N.		

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- Name:

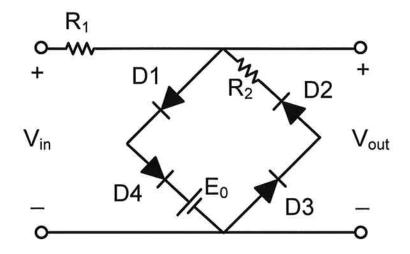
#### Question #1 (3 pts)

Two amplifier stages are connected in cascade to operate between a voltage source  $(v_s)$  with  $1M\Omega$  source resistance and a  $1k\Omega$  load. The <u>first amplifier stage</u>, which is a <u>voltage amplifier</u>, has an input resistance of  $500k\Omega$ , an open circuit voltage gain of 200V/V, and an output resistance of  $80k\Omega$ . The <u>second stage</u>, which is a <u>transconductance amplifier</u>, has an input resistance of  $100k\Omega$ , an output resistance of  $20k\Omega$ , and a short circuit transconductance of 5mA/V.

- a) Draw the entire circuit model from the voltage source to the  $1k\Omega$  load. (1 pt)
- b) What is the overall voltage gain,  $v_{out}/v_s$ .  $v_{out}$  is the voltage measured across the load.(1 pt)
- c) Consider the output current is  $i_0$ . What is the overall transconductance gain,  $i_0/v_s$ , if we replace the  $1k\Omega$  load resistor with a short circuit? (1 pt)

## Question #2 (6 pts)

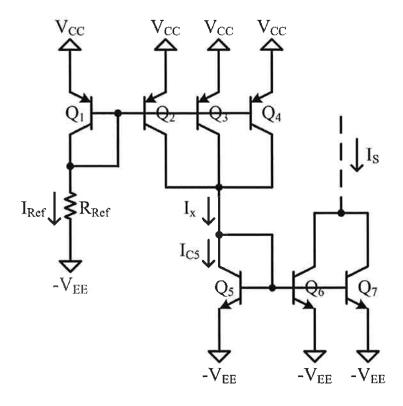
In the following circuit,  $R_1$ = 150 $\Omega$ ,  $R_2$ = 100 $\Omega$ ,  $E_0$ =1.6V. All the diodes are the same with  $V_D(on)$ = 0.7V. The small signal resistance of each diode in forward bias is 25 $\Omega$ .



- a) If the input voltage is  $V_{in} = 5 + 0.001 \times \cos(2\pi t)$  V, find the DC and AC output voltages, i.e.  $V_{out} = V_{out}(DC) + V_{out}(AC)$ . (3 pts)
- b) If the DC level of the input voltage is changed to -5V as given in  $V_{in} = -5 + 0.001 \times \cos(2\pi t)$  V, find the DC and AC output voltages, i.e.  $V_{out} = V_{out}(DC) + V_{out}(AC)$ . (3 pts)

## Question #3 (5 pts)

Consider the following BJT current steering circuit. All npn transistors are identical with  $\underline{\beta_P} = 100$ , and all pnp transistors are identical with  $\underline{\beta_P} = 80$ . The operating mode for all transistors are assumed to be the active mode, and  $|V_{BE}| = 0.7$ .

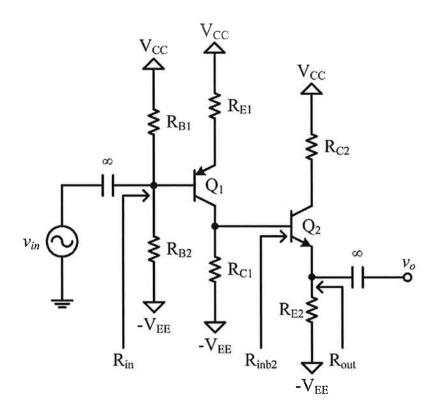


Considering  $I_S = 8mA$ ,  $V_{CC} = 5V$  and  $V_{EE} = 5V$ ,

- a) Calculate  $I_{C5}$  and  $I_x$ . (2 pts)
- b) Calculate  $I_{Ref}$  and  $R_{Ref}$ . (3 pts)

#### Question 4 (7 pts)

Consider the following two-stage BJT amplifier. You can assume that all transistors are in active mode and that they have the same  $\beta$ . The early effect for both transistors can be ignored.



- a) Draw the small signal model of the above circuit. (2 pts)
- b) Find an expression for R<sub>in</sub>. (1 pt)
- c) Find an expression for R<sub>inb2</sub>. (1 pt)
- d) Find an expression for R<sub>out</sub>. (1 pt)
- e) Derive an expression for  $v_o/v_{in}$ . (2 pts)

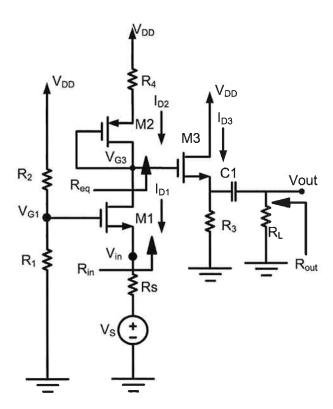
#### Question #5 (11 pts)

In the following circuit, all NMOS and PMOS transistors are operating in the saturation region. Assume  $R_1 = 200k\Omega$ ,  $R_2 = 400k\Omega$ ,  $R_3 = 2k\Omega$ ,  $R_4 = 1k\Omega$ ,  $R_L = 3k\Omega$ ,  $R_S = 1k\Omega$ .

The transistor parameters are  $\mu_n C_{OX} = 100 \mu A/V^2$ ,  $\mu_p C_{OX} = 50 \mu A/V^2$ ,  $V_{tn} = -V_{tp} = 0.5V$ ,  $(W/L)_1 = (W/L)_3 = 10$ , and  $(W/L)_2 = 20$ .

The supply voltage is  $V_{DD} = 6$  V. The DC voltage at the source of M1 is zero, i.e.  $Vin(DC) = V_{S1}(M1) = 0$ .

Note that the body effect and channel length modulation can be ignored in DC and small signal analysis.

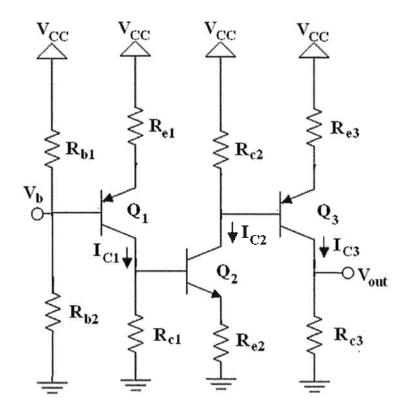


- a) Calculate  $V_{G1}$ ,  $I_{D1}$ ,  $I_{D2}$ ,  $V_{G3}$ , and  $I_{D3}$  and verify that all transistors are operating in the saturation mode.(5 pts)
- b) Derive an expression for  $R_{eq}$  and draw the small signal model of the entire circuit. No need to calculate the numerical values. (2 pts)
- c) Derive expressions for R<sub>out</sub>, R<sub>in</sub> and V<sub>out</sub>/V<sub>S</sub>. No need to calculate the numerical values. (4 pts)

#### Question 6 [8 pts]:

In the following circuit:

 $R_{b1}=3k\Omega$ ,  $R_{b2}=7k\Omega$ ,  $R_{e1}=2.25k\Omega$ ,  $R_{c1}=5k\Omega$ ,  $R_{e2}=2.25k\Omega$ ,  $R_{c2}=2k\Omega$ ,  $R_{e3}=3.3k\Omega$ ,  $R_{c3}=2k\Omega$ ,  $V_{CC}=10V$ , and  $\beta=50$  for all transistors. The Early effect can be ignored for all transistors.

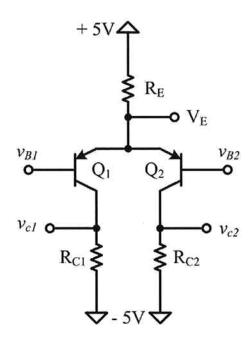


Find the values for  $V_b$ ,  $I_{C1}$ ,  $I_{C2}$ ,  $I_{C3}$ , and  $V_{out}$  and verify your assumption about the mode of operation of all transistors. (8 pts)

## Question 7 [10 pts]:

Consider the following differential amplifier circuit. Assume that all BJTs are identical and have  $|V_{BE}| = 0.7$  V. The Early effect can be ignored for all transistors. The input terminals are  $v_{BI}$  and  $v_{B2}$ , the differential input is  $v_d = v_{BI} - v_{B2}$  and the output terminals are  $v_{CI}$  and  $v_{C2}$ .

$$R_{C1} = R_{C2} = 2k\Omega$$
  
 $R_E = 5k\Omega$   
 $\beta = 99$  for all BJTs



- a) If  $V_{B1}$ = -0.8V and  $V_{B2}$ = 0.2V, find  $V_E$ ,  $V_{C1}$  and  $V_{C2}$ . (2 pts)
- b) If  $V_{B1}$ = 0.5V and  $V_{B2}$ = 0.5V, find  $V_E$ ,  $V_{C1}$  and  $V_{C2}$ . (2 pts)
- c) Draw the small signal model for this circuit. (2 pts)
- d) <u>Derive expressions</u> for the differential voltage gain, differential input resistance, differential output resistance and the Common mode gain. Considering the base voltages indicated in part (b), <u>calculate</u> the numerical values for these four parameters. (3 pts)
- e) If the output is connected to a resistive load  $R_L$ = 20 k $\Omega$ , i.e.  $R_L$  is connected between  $v_{c1}$  and  $v_{c2}$  terminals, calculate the new differential voltage gain. (1 pt)

Diodes: 
$$i=I_S(exp(v/nV_T)-1)$$

FETs:

NMOS:

$$V_{GS} < V_t$$
  $I_D = 0$ 

$$I_D = 0$$

$$V_{GS} > V_{t}$$

$$V_{GS} > V_{t}$$
  $I_{D} = k_{n}^{t} \frac{W}{L} [(V_{GS} - V_{t})V_{DS} - \frac{1}{2}V_{DS}^{2}]$   
 $V_{DS} < V_{GS} - V_{t}$ 

$$V_{GS} > V_{t}$$
 $V_{DS} > V_{CS} - V_{t}$ 

$$V_{t} = V_{t0} + \gamma \left( \sqrt{2\phi_{f} + V_{SB}} - \sqrt{2\phi_{f}} \right)$$

PMOS:

$$V_{GS} > V_t$$

$$I_D = 0$$

$$V_{GS} < V_t$$

$$I_D = k_p^t \frac{W}{L} [(V_{GS} - V_t)V_{DS} - \frac{1}{2}V_{DS}^2]$$

$$V_{DS} > V_{GS} - V_t$$

Saturation: 
$$V_{GS} < V_{\iota}$$

$$V_{DS} < V_{GS} - V_t$$

$$I_D = \frac{1}{2} k_p' \frac{W}{L} (V_{OS} - V_i)^2 (1 + \lambda V_{DS})$$

$$\left|V_{i}\right| = \left|V_{i0}\right| + \gamma \left(\sqrt{2\phi_{f} + \left|V_{SB}\right|} - \sqrt{2\phi_{f}}\right)$$

SMALL SIGNAL

$$g_m = \frac{2 \cdot I_D}{V_{GS} - V_L}$$

$$g_m = k_n^t \frac{W}{L} (V_{GS} - V_t) (1 + \lambda \cdot V_{DS})$$

$$g_{m} = \sqrt{2k_{n}'}\sqrt{\frac{W}{L}}\sqrt{1 + \lambda \cdot V_{DS}}\sqrt{I_{D}}$$

$$r_o = \frac{1}{\lambda \cdot I_D}$$

$$g_{mb} = \chi \cdot g_{m}$$

$$\chi = \frac{\gamma}{2} \cdot \frac{1}{\sqrt{2\phi_{c} + V_{cp}}}$$

Two-Page Formula Sheet

BJTs:

$$i_C = I_S \exp(v_{BE}/V_T)$$

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$$i_B = \frac{i_C}{\beta}$$

$$i_E = \frac{i_C}{\alpha}$$

$$i_B = (1 - \alpha)i_E = \frac{i_E}{\beta + 1}$$

$$i_E = (\beta + 1)i_B$$

$$g_m = \frac{I_C}{V_T}$$
  $r_e = \frac{V_T}{I_E} = \alpha \frac{V_T}{I_C} = \frac{\alpha}{g_m}$ 

$$r_{\pi} = \frac{V_T}{I_B} = \frac{\beta}{g_m} \quad r_o = \frac{V_A}{I_C}$$

$$r_{\pi} = (\beta + 1)r_{e}$$

$$\beta = \frac{\alpha}{1-\alpha} \alpha = \frac{\beta}{\beta+1} \beta+1 = \frac{1}{1-\alpha}$$