

PROBLEM SET #6

5-3, 5-8, 5-9, 6-3, 6-6

5-3

$R_1 = \text{resistance per unit length of core} = \frac{1}{\sigma S_1} = \frac{1}{\sigma \pi a^2}$

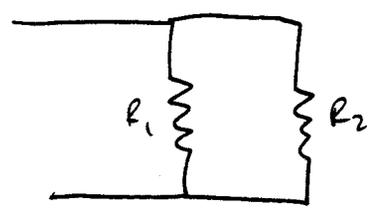
$R_2 = \text{resistance per unit length of coating} = \frac{1}{(0.1\sigma) S_2}$

let  $b = \text{thickness of coating} \rightarrow S_2 = \pi(a+b)^2 - \pi a^2$   
 $S_2 = \pi(2ab + b^2)$

a) 2 resistances are in parallel.

To make the resistance per unit length of the wire reduce by 50%, put a resistance in parallel so that  $R_1 = R_2$ .

Why



$R_{eq} = \frac{R_1 R_2}{R_1 + R_2}$

$R_{eq} = \frac{1}{2} R_1 = \frac{R_1 R_2}{R_1 + R_2}$

$\frac{1}{2} R_1 + \frac{1}{2} R_2 = R_2$

$\frac{1}{2} R_2 = \frac{1}{2} R_1 \rightarrow \underline{\underline{R_2 = R_1}}$

$$R_1 = R_2$$

$$\frac{1}{\cancel{\sigma} \pi a^2} = \frac{1}{(0.1\cancel{\sigma}) \pi (2ab + b^2)}$$

$$b^2 + 2ab - 10a^2 = 0$$

$$b = \frac{-2a \pm \sqrt{4a^2 - (4 \times (-10a^2))}}{2}$$

$$b = -a \pm \sqrt{11}a = a(\sqrt{11} - 1)$$

$$b = a(\sqrt{11} - 1) = 2.32a$$

b)  $I_1 = I_2 = \frac{I}{2} \rightarrow$  why, current divides equally into 2 branches of equal resistance.

$$J_1 = \frac{I_1}{\pi a^2} = \frac{I}{2\pi a^2}$$

$$J_2 = \frac{I_2}{S_2}$$

$$S_2 = ?$$

$$S_2 = \pi(a+b)^2 - \pi a^2$$

$$S_2 = \pi(a + \sqrt{11}a - a)^2 - \pi a^2$$

$$S_2 = 10a^2\pi$$

$$\rightarrow \text{so } J_2 = \frac{I_2}{10\pi a^2} = \frac{I}{20\pi a^2}$$

$$E_1 = \frac{J_1}{\sigma} = \frac{I}{2\pi a^2 \sigma}$$

$$E_2 = \frac{J_2}{0.1\sigma} = \frac{I}{2\pi a^2 \sigma}$$

so  $J_1 = 10J_2$  &  $E_1 = E_2$

(4b)

5-8

$$a) \quad R = \frac{l}{\sigma S} = \frac{V}{I} \longrightarrow \sigma = \frac{lI}{SV}$$

$$\sigma = \frac{(1000) \cdot (\frac{1}{b})}{(\pi(0.5 \times 10^{-3})^2)(b)} = 3.54 \times 10^7 \left(\frac{S}{m}\right)$$

$$b) \quad E = \frac{V}{l} = \frac{6 \text{ V}}{1000 \text{ m}} = 6 \times 10^{-3} \left(\frac{V}{m}\right)$$

$$c) \quad P = VI = 6 \text{ V} \times \frac{1}{6} \text{ A} = 1 \text{ (W)}$$

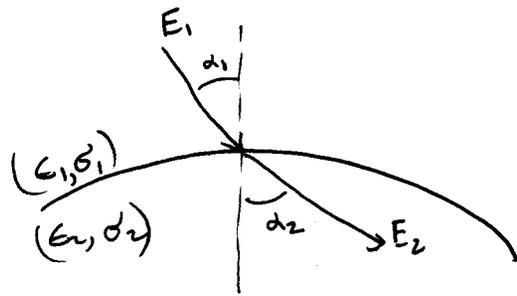
$$d) \quad \rho_e = -\frac{\sigma}{\mu_e} \quad \mu_e = 1.4 \times 10^{-3} \text{ m}^2/\text{Vs}$$

$$u = \left| \frac{J}{\rho_e} \right| = \left| \frac{\mu_e J}{\sigma} \right| = \left| \mu_e E \right| = 1.4 \times 10^{-3} \times 6 \times 10^{-3}$$

$$u = 8.4 \times 10^{-6} \left(\frac{m}{s}\right)$$

5-9

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a)  $E_2 = ?$

$$E_{1t} = E_{2t} \rightarrow E_1 \sin \alpha_1 = E_2 \sin \alpha_2$$

$$J_{in} = J_{zn} \rightarrow \sigma_1 E_{1n} = \sigma_2 E_{2n} \rightarrow \sigma_1 E_1 \cos \alpha_1 = \sigma_2 E_2 \cos \alpha_2$$

$$E_2^2 \sin^2 \alpha_2 = E_1^2 \sin^2 \alpha_1$$

$$+ \quad -E_2^2 \cos^2 \alpha_2 = \frac{\sigma_1^2}{\sigma_2^2} E_1^2 \cos^2 \alpha_1$$

$$E_2^2 = E_1^2 \sin^2 \alpha_1 + \frac{\sigma_1^2}{\sigma_2^2} E_1^2 \cos^2 \alpha_1$$

$$\therefore E_2 = E_1 \sqrt{\sin^2 \alpha_1 + \left(\frac{\sigma_1}{\sigma_2} \cos \alpha_1\right)^2}$$

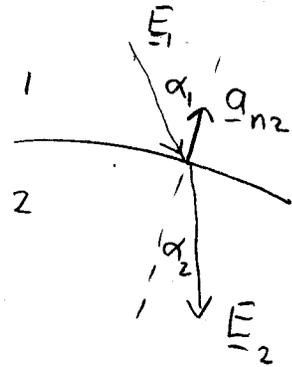
$$\tan \alpha_2 = \frac{\sigma_2}{\sigma_1} \tan \alpha_1 \rightarrow \alpha_2 = \tan^{-1} \left( \frac{\sigma_2}{\sigma_1} \tan \alpha_1 \right)$$

$$b) \quad \begin{pmatrix} D_1 \\ -1 \\ -2 \end{pmatrix} \cdot \underline{a}_{n2} = \rho_s$$

$$\Rightarrow \epsilon_1 E_{1n} - \epsilon_2 E_{2n} = \rho_s$$

$$\text{where } E_{1n} = \underline{E}_1 \cdot \underline{a}_{n2}$$

$$\& \quad E_{2n} = \underline{E}_2 \cdot \underline{a}_{n2}$$



$$\text{But } \sigma_2 E_{2n} = \sigma_1 E_{1n}, \text{ so } E_{2n} = \frac{\sigma_1}{\sigma_2} E_{1n}$$

$$\Rightarrow \rho_s = \left( \epsilon_1 - \epsilon_2 \frac{\sigma_1}{\sigma_2} \right) E_{1n}$$

$$\text{Now } E_{1n} = \underline{E}_1 \cdot \underline{a}_{n2} = -E_1 \cos \alpha_1 \quad (\text{see figure above})$$

$$\text{So } \rho_s = \left( \frac{\sigma_1}{\sigma_2} \epsilon_2 - \epsilon_1 \right) E_1 \cos \alpha_1$$

c) If both media are perfect dielectrics,  $\sigma_1 = \sigma_2 = 0$

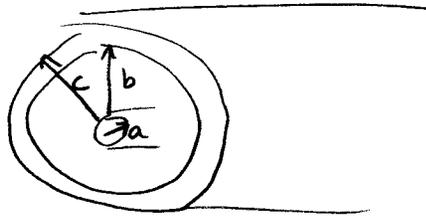
$$\& \quad \frac{\tan \alpha_2}{\tan \alpha_1} = \frac{\epsilon_2}{\epsilon_1}$$

$$\text{So } E_2 = E_1 \left[ \sin^2 \alpha + \left( \frac{\epsilon_1}{\epsilon_2} \cos \alpha_1 \right)^2 \right]^{\frac{1}{2}}$$

- eqn. (3-130) in Chapter 3

6-3

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Find  $\bar{B}$  for all regions.

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu I$$

Region 1:  
 $0 \leq r_1 \leq a$

$$\bar{B}_1 = a\hat{\phi} B_{\phi 1} \quad d\mathbf{l} = a\hat{\phi} r_1 d\phi$$

$$\oint_{C_1} B_1 \cdot d\mathbf{l} = \int_0^{2\pi} B_{\phi 1} a r_1 d\phi = 2\pi r_1 B_{\phi 1}$$

$$I_1 = \frac{\pi r_1^2}{\pi a^2} I$$

$$B_{\phi 1} = \frac{1}{2\pi r_1} \frac{\pi r_1^2}{\pi a^2} I \mu = \frac{\mu r_1 I}{2\pi a^2}$$

so

$$\bar{B} = a\hat{\phi} \frac{\mu r_1 I}{2\pi a^2} \quad 0 \leq r_1 \leq a$$

Region 2:

$$a \leq r_2 \leq b$$

$$\oint_{C_2} B_2 \cdot d\mathbf{l} = 2\pi r_2 B_{\phi 2}$$

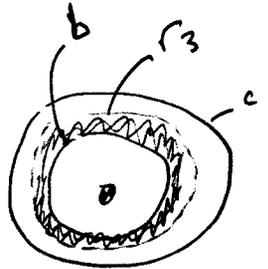
$$I_2 = I$$

$$B\phi_2 = \frac{1}{2\pi r_2} \cdot \mu I$$

so  $\bar{B} = a\bar{\phi} \frac{\mu I}{2\pi r_2} \quad a \leq r_2 \leq b$

Region 3:  
 $b \leq r_3 \leq c$

$$\oint_{C_3} B_3 \cdot dl = 2\pi r_3 B\phi_3$$



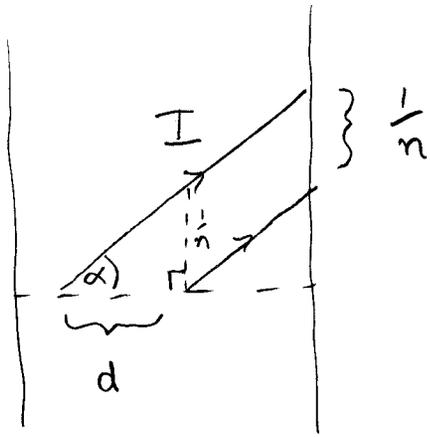
$I_3 = I - \frac{\pi r_3^2 - \pi b^2}{\pi c^2 - \pi b^2} I$  *from inside* → current of shaded part

$$I_3 = \frac{\pi c^2 - \pi b^2 - \pi r_3^2 + \pi b^2}{\pi c^2 - \pi b^2} I = \frac{\pi c^2 - \pi r_3^2}{\pi c^2 - \pi b^2} I$$

so  $\bar{B} = a\bar{\phi} \left( \frac{c^2 - r_3^2}{c^2 - b^2} \right) \frac{\mu I}{2\pi r_3} \quad b \leq r_3 \leq c$

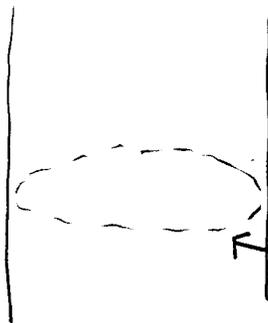
6-6

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$$\tan \alpha = \frac{n}{d}$$

$$\Rightarrow d = \frac{1}{n \tan \alpha}$$

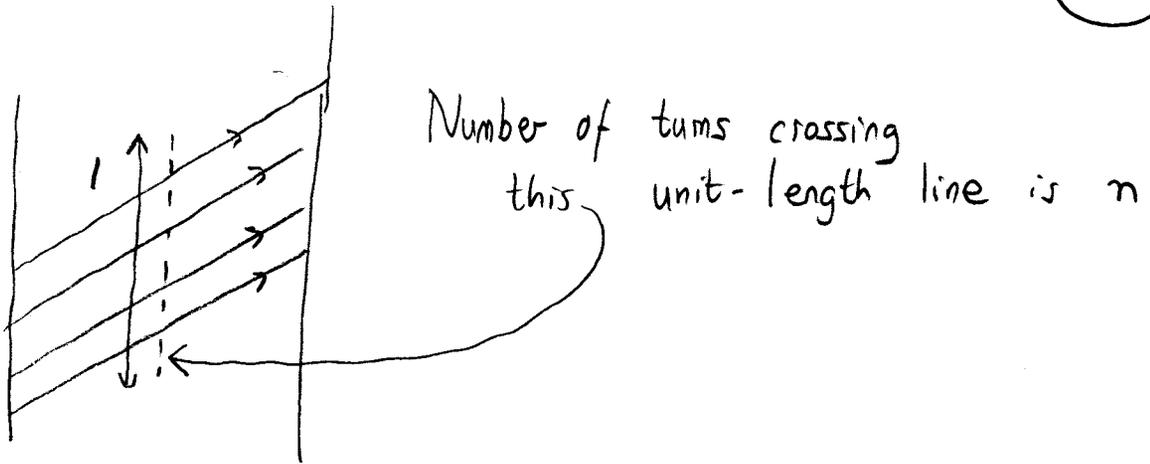


So number of turns

crossing this circle is  $\frac{2\pi b}{d}$ or  $2\pi b n \tan \alpha$ (NOT just  $2\pi b n$ )ie axial current,  $I_i$ , is  $I \times 2\pi b n \tan \alpha$ From Ampère's Law, the field  $B_i$  created by this is

$$2\pi r B_{i\phi} = \mu_0 2\pi b n I \tan \alpha$$

$$\Rightarrow B_{i\phi} = \begin{cases} \frac{b \mu_0 n I \tan \alpha}{r} & r > b \\ 0 & 0 < r < b \end{cases}$$



ie circumferential ( $\phi$ ) current,  $I_2$ , per unit length is  $nI$

But this is the same as a regular solenoid with  $n$  turns/m carrying current  $I$ .

From p. 231, Ex 6-3:

$$B_{2z} = \begin{cases} \mu_0 n I & 0 < r < b \\ 0 & r > b \end{cases}$$

Total field  $\underline{B}$  is  $\underline{B}_1 + \underline{B}_2$

$$= \begin{cases} \underline{a}_z \mu_0 n I & 0 < r < b \\ \underline{b} \mu_0 n I \frac{\tan \alpha}{r} & r > b \end{cases}$$