

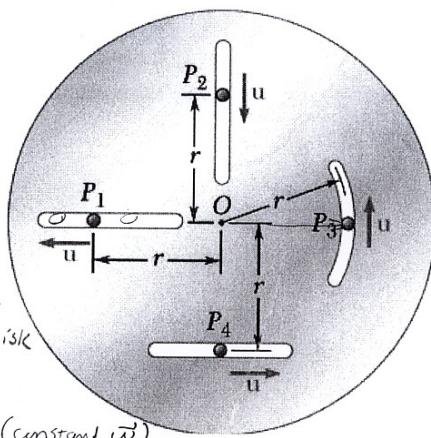
Solution to Assignment 6

$\frac{1}{10}$

CIVE 281

PROBLEM 15.156

Four pins slide in four separate slots cut in a circular plate as shown. When the plate is at rest, each pin has a velocity directed as shown and of the same constant magnitude u . If each pin maintains the same velocity relative to the plate when the plate rotates about O with a constant counterclockwise angular velocity ω , determine the acceleration of each pin.



Frame of reference placed
at position "O".
 $\therefore A_{xyz}$
is centered at center of disk

For all pins: $\dot{\omega} = \phi$ (constant ω)

$\ddot{\alpha}_A = \phi$ (no translation of ref. frame ... origin of fixed frame $Oxyz$ + reference frame $Axyz$ coincide)

$$\text{for pin 1: } \ddot{\alpha}_{P_1} = \ddot{\alpha}_A + \dot{\omega} \times \vec{r}_{P/A}^{\phi} - \vec{r}\hat{i} + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{P/A})^{\phi} + 2\vec{\omega} \times \dot{\vec{r}}_{P/A}^{\phi} + \ddot{\vec{r}}_{P/A}^{\phi}$$

where $\vec{\omega} = (0 \ 0 \ \omega)$

$$|\ddot{\alpha}_{P_1}| = \sqrt{rw^2 \hat{i}^2 - 2uw\hat{j}|}$$

$$\text{for pin 2: } \ddot{\alpha}_{P_2} = \ddot{\alpha}_A + \dot{\omega} \times \vec{r}_{P/A}^{\phi} - \vec{r}\hat{j} + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{P/A})^{\phi} + 2\vec{\omega} \times \dot{\vec{r}}_{P/A}^{\phi} + \ddot{\vec{r}}_{P/A}^{\phi}$$

$$|\ddot{\alpha}_{P_2}| = \sqrt{2uw\hat{i}^2 - rw^2\hat{j}|}$$

$$\text{for pin 4: } \ddot{\alpha}_{P_4} = \ddot{\alpha}_A + \dot{\omega} \times \vec{r}_{P/A}^{\phi} - \vec{r}\hat{j} + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{P/A})^{\phi} + 2\vec{\omega} \times \dot{\vec{r}}_{P/A}^{\phi} + \ddot{\vec{r}}_{P/A}^{\phi}$$

$$|\ddot{\alpha}_{P_4}| = \sqrt{(rw^2 + 2uw)\hat{j}|}$$

15.156 cont'd)

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$$\text{In pin 3 : } \vec{a}_{P_3} = \vec{a}_A^\phi + \dot{\omega} \times \vec{r}_{PA}^n + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{PA}^n) + 2\vec{\omega} \times \vec{r}_{PA}^u + \ddot{r}_{PA}$$

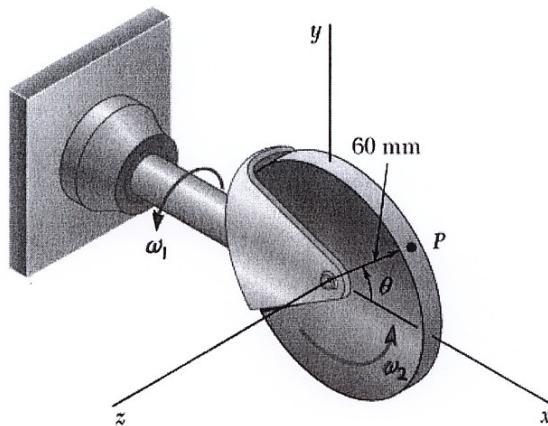
\ddot{r}_{PA} has a normal acceleration component because of the curved path.

$$\ddot{r}_{PA} \Rightarrow \frac{du}{dt} = \frac{d^2r}{dt^2} = u \frac{du}{dr} = -\frac{u^2}{r} \Rightarrow -\frac{u^2}{r} \uparrow$$

$$\boxed{\vec{a}_{P_3} = -(rw^2 + 2uw + \frac{u^2}{r}) \hat{z}}$$

PROBLEM 15.190

A 60-mm-radius disk spins at the constant rate $\omega_2 = 4 \text{ rad/s}$ about an axis held by a housing attached to a horizontal rod that rotates at the constant rate $\omega_1 = 5 \text{ rad/s}$. For the position shown, determine (a) the angular acceleration of the disk, (b) the acceleration of point P on the rim of the disk if $\theta = 0$, (c) the acceleration of point P on the rim of the disk if $\theta = 90^\circ$.



NOTE:

Two different locations of the frame of reference are used to solve part (a) + parts (b) and (c).

- (a) Reference frame is placed on the clamp (at the center of $x-y-z$ axis in the schematic). Thus it is not placed on the disk + $\vec{\omega}_2$ does NOT rotate with $\vec{\omega}_2$ but does rotate with $\vec{\omega}_1$.

This is done to facilitate the solution to the following equation:

$$\dot{\vec{Q}}_{Oxyz} = \dot{\vec{Q}}_{Anxyz} + \vec{\omega} \times \vec{Q}$$

15.190 cont'd)

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Now solve for $\vec{\omega}$:

$\vec{\omega} = \dot{\vec{\omega}} = \dot{\vec{\omega}}_1 + \dot{\vec{\omega}}_2$ but since A_{xyz} is on the clamp it rotates

$$\text{w/ } \dot{\vec{\omega}}_1 + \text{so } \dot{\vec{\omega}}_1 = \phi.$$

$$\text{Thus } \vec{\omega} = \dot{\vec{\omega}}_2$$

Now plug in $\dot{\vec{\omega}}_2$ as $\vec{\omega}$:

$$\begin{aligned}\dot{\vec{\omega}}_2_{\text{OXYZ}} &= \dot{\vec{\omega}}_{A_{xyz}} + \vec{\omega} \times \vec{\omega} \\ \dot{\vec{\omega}}_2 &= \dot{\vec{\omega}}_2^\phi + \vec{\omega}_1 \times \vec{\omega}_2 \quad \text{param of interest} \\ &\quad \text{L.R.T. ref frame ... } \vec{\omega}_2 = \text{constant } \text{so } \dot{\vec{\omega}}_2 = \phi \\ \dot{\vec{\omega}}_2 &= \vec{\omega}_1 \times \vec{\omega}_2 \\ \dot{\vec{\omega}}_2 &= \vec{\omega} = \dot{\vec{\omega}} = \boxed{-20 \hat{j} \text{ rad/s}}\end{aligned}$$

(b) + (c)

Reference frame is placed @ center of disk (thus A_{xyz} rotates with $\vec{\omega}_1 + \vec{\omega}_2$).

$$\vec{a}_P = \vec{a}_A + \vec{\omega} \times \vec{r}_{P/A} + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{P/A}) + 2\vec{\omega} \times \dot{\vec{r}}_{P/A} + \ddot{\vec{r}}_{P/A}$$

$(504) = \omega_1 + \omega_2 = \text{ans. vel. of ref frame } A_{xyz}$

part (b) $\theta = 0^\circ$

$$\therefore r = (60 \ 0 \ 0) \text{ mm}$$

$$+ \boxed{\vec{a}_P = -960 \hat{i} + 2400 \hat{k} \text{ mm/s}}$$

are ϕ because the point P does not move independent of the ref frame A_{xyz} ... i.e. The ref frame moves with both $\vec{\omega}_1 + \vec{\omega}_2$ & P does not move independent of the rotations (thus $\vec{r} + \dot{\vec{r}} = \phi$)

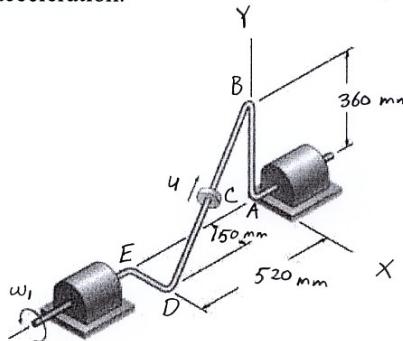
part (c) $\theta = 90^\circ$

$$\therefore r = (0 \ 60 \ 0) \text{ mm}$$

$$+ \boxed{\vec{a}_P = -2460 \hat{j} \text{ mm/s}}$$

PROBLEM 15.215

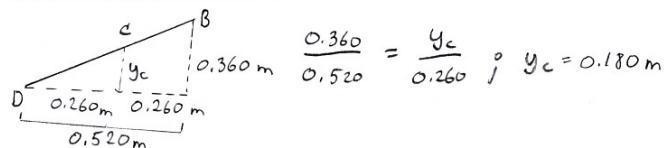
The bent rod shown rotates at the constant rate $\omega_1 = 5 \text{ rad/s}$ and collar C moves toward point B at a constant relative speed $u = 975 \text{ mm/s}$. Knowing that collar C is halfway between points B and D at the instant shown, determine its velocity and acceleration.



Place reference frame at point A on schematic.

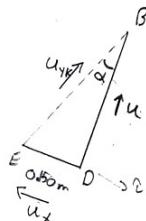
Need to solve for $\vec{r}_{C/A}$ + $\dot{\vec{r}}_{C/A}$ in order to solve the velocity + acceleration equations.

$$\vec{r}_{C/A} :$$



$$\therefore \vec{r}_{C/A} = (0.075\hat{i} + 0.180\hat{j} + 0.260\hat{k}) \text{ m}$$

$$\dot{\vec{r}}_{C/A} :$$



$$\bar{BO} = \sqrt{(0.150)^2 + (0.360)^2 + (0.520)^2} \\ = 0.650 \text{ m}$$

$$\alpha = 13.34^\circ$$

$$* \vec{U}_x = -(0.975 \sin(13.34)) = -0.225 \hat{i} \text{ m/s}$$

$$\vec{U}_{yK} = (0.975 \cos(13.34)) = 0.9487 \hat{j} \text{ m/s (direction in schematic)}$$



$$\beta = 34.69^\circ$$

$$* \vec{U}_y = \sin(34.69) \times 0.9487 = 0.540 \hat{j} \text{ m/s}$$

$$* \vec{U}_k = -\cos(34.69) \times 0.9487 = -0.778 \hat{k} \text{ m/s}$$

15.215 cont'd)

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$$\therefore \dot{\vec{r}}_{c/A} = \vec{u}_x + \vec{u}_y + \vec{u}_z \\ = (-0.225 \hat{i} + 0.540 \hat{j} - 0.778 \hat{k}) \text{ m/s}$$

Now use the velocity equation:

$$\vec{v}_c = \vec{v}_A + \vec{\omega} \times \vec{r}_{c/A} + \dot{\vec{r}}_{c/A} \\ \vec{\omega}_D = \vec{\omega}_1 = \text{ang vel of ref frame} = (0 \ 0 \ 5) \\ \vec{v}_c = \sqrt{-1.125^2 + 0.915^2 - 0.778^2}$$

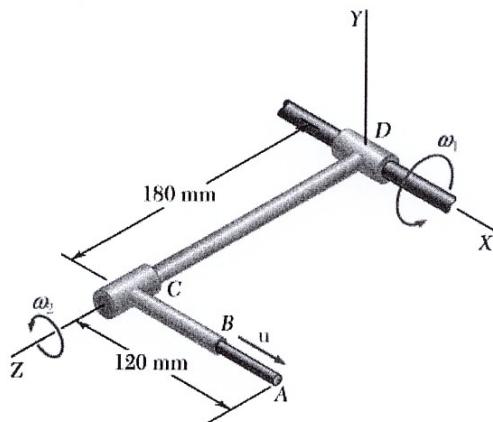
Now use the acceleration equation:

$$\vec{a}_c = \vec{g}_A^{n\phi} + \vec{\omega}_1 \times \dot{\vec{r}}_{c/A} + \vec{\omega}_1 \times (\vec{\omega}_1 \times \vec{r}_{c/A}) + 2\vec{\omega}_1 \times \dot{\vec{r}}_{c/A} + \ddot{\vec{r}}_{c/A} \\ \vec{a}_c = \sqrt{-7.28^2 - 6.75^2} \text{ m/s}^2$$

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PROBLEM 15.235

In the position shown the thin rod moves at a constant speed $u = 60 \text{ mm/s}$ out of the tube BC . At the same time tube BC rotates at the constant rate $\omega_2 = 1.5 \text{ rad/s}$ with respect to arm CD . Knowing that the entire assembly rotates about the X axis at the constant rate $\omega_1 = 1.2 \text{ rad/s}$, determine the velocity and acceleration of end A of the rod.



Velocity \vec{v}_A

Frame of reference centered at point D , on rigid body DCB .

$$\therefore \vec{\omega} = \vec{\omega}_1 + \vec{\omega}_2 = 1.2\hat{i} + 1.5\hat{k} \text{ rad/s}$$

$$\vec{v}_A = \vec{v}_D + \vec{v}_{A/D} + \dot{\vec{r}}_{A/D}$$

↓
D translation of ref frame

$$= \vec{v}_D + \vec{\omega} \times \vec{r}_{A/D} + \dot{\vec{r}}_{A/D}$$

$$= (1.2\hat{i} + 1.5\hat{k}) \times (0.120\hat{i} + 0.180\hat{k}) \text{ m/s} + \dot{\vec{r}}_{A/D}$$

Aside $\vec{r}_{A/D} = \text{rel of } A \text{ relative to the ref. frame.}$

$$\therefore \vec{r}_{A/D} = u\hat{i} = 0.06 \text{ m/s} \hat{i}$$
$$\vec{v}_A = \begin{pmatrix} 1.2 & 1.5 \\ 0.120 & 0.180 \end{pmatrix} + (0.06 \ 0 \ 0) = \underline{\underline{[0.06 \hat{i} - 0.036 \hat{j} \text{ m/s}]}}$$

15.235 cont'd)

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acceleration:

New reference frame: place reference frame at pt D such that
 $\vec{\omega} = \dot{\vec{\omega}}_1 + \dot{\vec{\omega}}_2$ it does not rotate with ω_2 but only rotates with
 since the ref frame rotates
 w/ ω_1 , then $\dot{\vec{\omega}}_1 = \phi$. ω_1 . (same as problem 15.190)

$$\text{so } \dot{\vec{\omega}} = \dot{\vec{\omega}}_2 \quad \text{w.r.t. ref frame}$$

$$\text{now use: } \dot{\vec{Q}}_{OXYZ} = \dot{\vec{Q}}_{Axyz} + \dot{\vec{\omega}} \times \vec{Q} \quad \begin{matrix} \text{vector Q w.r.t. OXYZ (fixed frame)} \\ \text{angular velocity of ref. frame} \end{matrix}$$

$$\text{where } \vec{Q} = \vec{\omega}_2$$

$$\dot{\vec{\omega}}_2 = \dot{\vec{\omega}}_2^\phi + (\vec{\omega}_1 \times \vec{\omega}_2)$$

$$\dot{\vec{\omega}}_2 = (1.2 \ 0 \ 0) \times (0 \ 0 \ 1.5)$$

$$\text{so } \dot{\vec{\omega}} = \dot{\vec{\omega}}_2 = -1.8 \hat{j} \text{ rad/s}$$

now solve for \vec{a}_A .

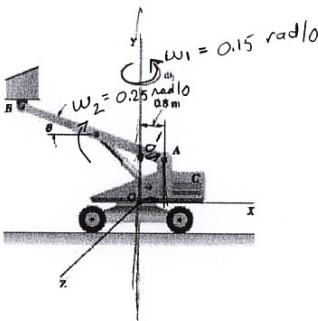
$$\vec{a}_A = \underbrace{\vec{a}_0^\phi}_{\substack{\text{Translation} \\ \text{of ref. frame}}} + \underbrace{\dot{\vec{\omega}} \times \vec{r}}_{\substack{\text{Tangential}}} + \underbrace{\vec{\omega} \times (\vec{\omega} \times \vec{r})}_{\substack{\text{normal}}} + 2\vec{\omega} \times \dot{\vec{r}}_{AO} + \ddot{\vec{r}}_{AO}$$

$$= \phi + (0 \ -1.8 \ 0) \times (120 \ 0 \ 180) + (1.2 \ 0 \ 1.5) \times [(1.2 \ 0 \ 1.5) \times (120 \ 0 \ 180)] + 2(1.2 \ 0 \ 1.5) \times (60 \ 0 \ 0)$$

$$\vec{a}_A = \boxed{-270 \hat{i} + 180 \hat{j} + 172.8 \hat{k} \text{ mm/s}^2}$$

PROBLEM 15.254

The arm AB of length 5 m is used to provide an elevated platform for construction workers. In the position shown, arm AB is being raised at the constant rate $d\theta/dt = 0.25 \text{ rad/s}$; simultaneously, the unit is being rotated counterclockwise about the Y axis at the constant rate $\omega_1 = 0.15 \text{ rad/s}$. Knowing that $\theta = 20^\circ$, determine the velocity and acceleration of point B .



Reference frame rotates
with $\vec{\omega}_1$ but not $\vec{\omega}_2$
 $\vec{\omega}_2$ @ position Axyz.

velocity:

$$\vec{v}_B = \vec{v}_A + \vec{\omega}_1 \times \vec{r}_{B/A} + \dot{\vec{r}}_{B/A}$$

\vec{v}_A = translation of reference frame (ie translation of ref. frame from pt O to pt A)

$$= \vec{\omega}_1 \times \vec{r}_{O/A}$$

$\dot{\vec{r}}_{B/A}$ = vel of B relative to the reference frame (since B has a rotation of $\vec{\omega}_2$ independent of Axyz - rotates with $\vec{\omega}_1$)

$$= \vec{\omega}_2 \times \vec{r}_{B/A}$$

$$\vec{v}_B = \vec{\omega}_1 \times \vec{r}_{O/A} + \vec{\omega}_1 \times \vec{r}_{B/A} + \vec{\omega}_2 \times \vec{r}_{B/A}$$

$$= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0.15 & 0 \\ 0.8 & 0 & 0 \end{vmatrix} + \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0.15 & 0 \\ -4.7 & 1.71 & 0 \end{vmatrix} + \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & -0.25 \\ -4.7 & 1.71 & 0 \end{vmatrix} = \boxed{\begin{matrix} -0.428\hat{i} + 1.175\hat{j} \\ + 0.585\hat{k} \end{matrix} \text{ m/s}}$$

15.254 cont'd)

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acceleration:

$$\vec{a}_B = \vec{a}_A + \overset{\circ}{\omega}_1 \times \vec{r}_{B/A} + \vec{\omega}_1 \times (\vec{\omega}_1 \times \vec{r}_{B/A}) + 2\vec{\omega}_1 \times \dot{\vec{r}}_{B/A} + (\ddot{\vec{r}}_{B/A})$$

$$\vec{a}_A = \vec{\omega}_1 \times (\vec{\omega}_1 \times \vec{r}_{A/I})$$

$$\dot{\vec{r}}_{B/A} = \vec{\omega}_2 \times \vec{r}_{B/A}$$

$$\ddot{\vec{r}}_{B/A} = \vec{\omega}_2 \times (\vec{\omega}_2 \times \vec{r}_{B/A}) = \vec{\omega}_2 \times \dot{\vec{r}}_{B/A}$$

$$\begin{aligned} \overset{\circ}{\omega} \vec{a}_B &= \vec{\omega}_1 \times (\vec{\omega}_1 \times \vec{r}_{A/I}) + \vec{\omega}_1 \times (\vec{\omega}_1 \times \vec{r}_{B/A}) + 2\vec{\omega}_1 \times (\vec{\omega}_2 \times \\ &\quad + \vec{\omega}_2 \times (\vec{\omega}_2 \times \vec{r}_{B/A})) \end{aligned}$$

$$\vec{a}_B = \sqrt{0.381 \hat{x} + 0.1069 \hat{y} - 0.1283 \hat{z}} \text{ m/s}^2$$